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The GEOS-5 Data Assimilation System - Documentation of Versions 5.0.1, 5.1.0, and 5.2.0.

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DRAFT

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1. Introduction

The assimilation system described in this document is a major new version of the Goddard Earth Observing System Data Assimilation System (GEOS DAS) based on the GEOS-5 Atmospheric General Circulation Model (AGCM) with the Gridpoint Statistical Interpolation (GSI) Analysis. The GEOS DAS has evolved over a number of years, with the primary milestones driven by major launches of the EOS series of satellites. The evolving system to GEOS-4, with the science and application drivers, were described in Bloom et al. (2005).

The GEOS-5 DAS represents a radical evolution of the system, with the adoption of a joint analysis with the National Centers for Environmental Prediction (NCEP) and of a new set of physics packages for the atmospheric general circulation model (AGCM). The first choice allows the Global Modeling and Assimilation Office (GMAO) to take advantage of the developments, especially that of radiance assimilation, at NCEP and the Joint Center for Satellite Data Assimilation (JCSDA), and facilitates our own contributions to the operational system. The second choice allows us to tune the system for both weather and climate applications, taking advantage of satellite observations in the assimilation context as we do so.

The new GEOS-5 AGCM maintains the finite-volume dynamics (Lin, 2004) used for GEOS-4 and found to be so effective especially for transport in the stratosphere. This dynamical core is integrated with various physics packages under the Earth System Modeling Framework (ESMF) (e.g., Collins et al., 2005) including the Catchment Land Surface Model (CLSM) (e.g., Koster et al., 2000). The GSI analysis is a new three-dimensional variational (3DVar) analysis applied in grid-point space to facilitate the implementation of anisotropic, inhomogeneous covariances (e.g., Wu et al., 2002; Derber et al., 2003; Parrish et al., 2003). GMAO scientists have contributed to GSI development since 2004.

During implementation in GEOS-5, this system has continued along its development path. One result of this was the need to address shocks introduced by imbalances in the mass-wind analysis increments. Although balance constraints are under development, in order to meet the GMAO's production schedule requirements, the decision was made to re-introduce (from GEOS-3) the incremental analysis update (IAU) procedure (Bloom et al., 1996) and this has proven very effective.

The primary performance drivers for the production of GEOS DAS assimilation fields are temperature and moisture fields suitable for the EOS instrument teams, wind fields for the transport studies of the stratospheric and tropospheric chemistry communities, and climate-quality analyses to support studies of the hydrological cycle through the Modern Era Reanalysis for Research Applications (MERRA, e.g., Bosilovich et al., 2006). Other significant drivers for the GEOS DAS have involved the provision of near real-time mission support for a number of atmospheric chemistry mission field campaigns.

This report documents Version 0.1 of GEOS-5, also referred to as GEOS-5.0.1, the interim release used to meet the production timeline requirements of the EOS instrument teams. The upgrades implemented for Version 1.0, referred to as GEOS-5.1.0, which address some of the deficiencies noted by the instrument teams and in our tuning of the DAS for MERRA are documented as are those for Version 2.0, referred to as GEOS-5.2.0, which addresses some additional deficiencies noted by the CERES science team and some final model tuning and analysis upgrades for MERRA.

This system documentation is organized as follows: The main characteristics of the atmospheric model are described in Chapter 2. The analysis system is described in Chapter 3. The assimilation system and observing system details are described in Chapter 4. The specific upgrades from GEOS-5.0.1 to GEOS-5.2.0 are documented in Chapter 5.

2. The GEOS-5 Atmospheric General Circulation Model

The GEOS-5 atmospheric model is a weather-and-climate capable model being used for atmospheric analyses, weather forecasts, uncoupled and coupled climate simulations and predictions, and for coupled chemistry-climate simulations. The applications have used model configurations from 2° to 1/4° resolutions, with 72 layers to 0.01 hPa, resolving both the troposphere and the stratosphere. The AGCM relies heavily on both ESMF superstructure and infrastructure for its internal architecture (e.g., Collins et al., 2005). Parallelization is primarily implemented through MPI, although some key parts of the code, such as the model dynamics, also have Open-MP capability. The model runs on a 2-D decomposition, transposing internally between horizontal and vertical layouts. Some of the physics such as the solar radiation, which at any given time is active over only half the globe, is load balanced. The code scales well across compute nodes and scalability increases linearly with problem size.

Developments of GEOS-5 were guided by a realistic representation of tracer transports and stratospheric dynamics. The ozone analysis of the DAS is input to the radiation package along with an aerosol climatology. GEOS-5 is coupled to a catchment-based hydrologic model (Koster et al., 2000) and a sophisticated multi-layer snow model (Stieglitz et al., 2001) that is coupled to the catchment hydrology. The land-surface albedos are derived from MODIS retrievals (Moody et al., 2005).

2.1 Hydrodynamics

The finite-volume dynamical core has an extensive documentation in the open literature (e.g., Lin 2004, and references therein). The difference from the GEOS-4 implementation is merely a technical computational issue of layout on processing elements. GEOS-5 uses a 2-D horizontal decomposition.

2.2 Physics

The physics package includes four major groups of physical processes: moist processes, radiation, turbulent mixing, and surface processes. Each of these in turn is subdivided into various components. The radiation module includes longwave radiation, and shortwave radiation. The turbulent mixing consists of the vertical diffusion, planetary boundary layer parameterization, and gravity wave drag. The surface processes provide surface fluxes obtained from land, ocean and sea ice models.

2.2.1 Moist Physics Parameterizations

In developing GEOS-5, attention has focused on the representation of moist processes. GEOS5_Moist considers liquid and ice phases of cloud condensate. Two separate cloud "types" are also recognized explicitly, with separate fraction and condensate variables kept for each type. The cloud types are distinguished by their source. One type, which will be denoted "anvil" cloud, originates in detraining convection. The second type, which is referred to as large-scale cloud, originates in a probability distribution function (PDF) based condensation calculation. Once created, condensate and fraction from the anvil and large-scale cloud types experience the same loss processes: evaporation, autoconversion, sedimentation and accretion. Parameter settings may vary by type, but identical formulations are used. Clouds associated with updraft cores are not treated prognostically, but rainfall from convective cores is disposed of within GEOS5 Moist.

Table 2.2.1: Principal quantities appearing in the GEOS5_Moist physics package. Quantities labeled "input/output" are AGCM prognostic fields that incur modifications due to moist processes. Normally, these fields are also modified by other model processes, e.g., advection. Those labeled "internal" are not modified by processes outside of GEOS5_Moist, and normally are not prognostic, that is, they are generated and disposed of within a single call to GEOS5_Moist. These fields are important in the internal dynamics of GEOS5_Moist but are normally not required by other model processes. Fields labeled "output" are products of GEOS5_Moist for other GEOS5 processes. These are used but may not be modified by other processes.

Variable	Description	Status
и	Zonal wind	Input/output
v	Meridional wind	Input/output
T	Air temperature	Input/output
q	Specific humidity	Input/output
$q_{l,ls}$	Liquid cloud condensate large scale source (LS)	Input/output
$q_{i,ls}$	Frozen cloud condensate (LS)	Input/output
$q_{l,an}$	Liquid cloud condensate anvil source (AN)	Input/output
$q_{i,an}$	Frozen cloud condensate (AN)	Input/output
f_{ls}	Cloud fraction (LS)	Input/output
f_{an}	Cloud fraction (AN)	Input/output
$q_{p,l,ls}$	Liquid precipitating condensate (LS)	Internal
$q_{p,i,ls}$	Frozen precipitating condensate (LS)	Internal
$q_{p,l,an}$	Liquid precipitating condensate (AN)	Internal
$q_{p,i,an}$	Frozen precipitating condensate (AN)	Internal
$q_{c,cu}$	Total (ice+liquid) cloud condensate in cumulus updrafts (CU)	Internal
$q_{p,c,cu}$	Total precipitating condensate (CU)	Internal
$q_{p,l,cu}$	Liquid precipitating condensate (CU)	Internal
$q_{p,i,cu}$	Frozen precipitating condensate (CU)	Internal
f_{cu}	Areal fraction of cumulus updrafts	Internal
ϕ_{cu}	Mass flux in cumulus updrafts	Internal
P_{cu}	Surface flux of precipitation from cumulus updrafts	Output
P_{an}	Surface flux of precipitation from anvils	Output
P_{ls}	Surface flux of precipitation from large scale clouds	Output

The basic sequence of events in GEOS5_Moist is as follows. First, the convective parameterization, Relaxed Arakawa-Schubert, or RAS (Moorthi and Suarez, 1992) is called. RAS estimates convective mass fluxes for a sequence of idealized convective plumes. Each plume produces detraining fluxes of mass and cloud condensate, as well as profiles of precipitating condensate. Adjustments to the environmental profiles of u, v, T and q are also calculated sequentially by each plume.

Next, the large-scale cloud condensate scheme (PrognoCloud) is called. PrognoCloud first takes the detraining mass and condensate fluxes from RAS, if any exist, and adds them to the existing condensate and fraction of the anvil cloud type. Next, large-scale condensation is estimated using a simple assumed PDF of q_{total} . This step produces a new fraction and condensate for the large-scale cloud type. Freezing of existing cloud condensate and partitioning of the new cloud condensate are also performed for both cloud types.

After all sources of cloud condensate have been taken into account, four loss mechanisms are invoked: 1) Evaporation of condensate and fraction, 2) Autoconversion of liquid or mixed phase condensate, 3) sedimentation of frozen condensate and 4) Accretion of condensate by falling precipitation. Each of these

losses is applied to both anvil and statistical cloud types. The formulation of these terms is detailed below.

In addition to producing and disposing of condensate, PrognoCloud handles the fallout of autoconverted (precipitating) condensate. Precipitating condensate is accumulated from the top down. In each model layer a typical drop size, fall speed, and residence time is estimated. These parameters are used to estimate re-evaporation of falling precipitation. These calculations are done separately for precipitation originating from each of the two cloud types, as well as for convective core precipitation. A profile of autoconverted condensate averaged over the grid-box within convective updrafts is one of the outputs of RAS.

A schematic diagram of GEOS5_Moist is shown in Figure 2.2.1. Each process within GEOS5_Moist is discussed in greater detail below.

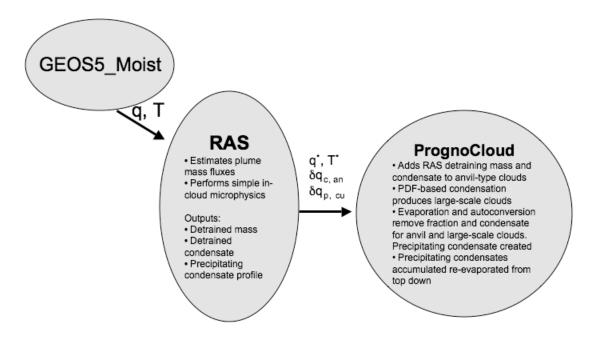


Figure 2.2.1: Schematic of Moist processes in GEOS-5.

2.2.1.1 Convection

GEOS5_Moist uses a modified version of the scheme described by Moorthi and Suarez (1992). As in Moorthi and Suarez a sequence of linearly entraining plumes is considered with mass flux profiles given by

$$\phi_k(z) = \phi_{0k}(1 + \lambda_k z).$$

The entrainment parameter for the k-th plume, λ_k , is determined by the choice of cloud base and cloud detrainment level. The GEOS-5 implementation is flexible in this respect. The default is to take an average of the two lowest model layers as the cloud-base layer. In GEOS-5 each model layer is tested, starting from the model level near 100 hPa and moving down to the level above cloud base. A random

selection of plumes is also possible. However, this choice does not appear to have a major impact on model behavior as long as roughly similar numbers of plumes are invoked.

Once cloud base, detrainment level, and λ_k have been chosen, a series of calculations is made for the plume. A modified CAPE-based closure is used to determine the cloud base mass flux, ϕ_{0k} . In addition to determining, ϕ_{0k} and λ_k a steady state profile of vertical velocity w_k is determined for each plume as first suggested by Sud and Walker (1999). The calculation of w_k in GEOS-5 is simpler than that of Sud and Walker: the buoyancy force is vertically integrated from cloud base to detrainment level to obtain a velocity profile which is multiplied by an empirical tuning parameter

$$w_k = \alpha_{w,cu} \int_{z_B}^{z_D} g \frac{\bar{T}_k - T_0}{T_0} dz$$
.

This approximate approach is employed because of the severe limitations inherent in the plume/parcel view of convection, including the neglect of pressure forces on the parcel.

Autoconversion of convective condensate, $q_{c,cu}$, to precipitating condensate, $q_{p,c,cu}$, is also treated following Sud and Walker (1999). Once an updraft velocity profile $w_k(z)$ is estimated for each plume it is used to derive time-scales $\Delta z_k/w_k$ for parcels rising through the plume, which are then employed in simple temperature-dependent, Sundquist-type expressions for autoconversion

$$\delta q_{p,c,cu,k} = -\delta q_{c,cu,k} \approx C_{0,cu} f(T) \left\{ 1 - \exp \left(\frac{-q_{c,cu,k}^2}{q_{c,crit}^2 / f(T)^2} \right) \right\} q_{c,cu,k} \bullet \frac{\Delta z_k}{w_k}.$$

Here $C_{0,cu}$ is a base autoconversion rate for condensate in convective plumes. It is multiplied by a temperature dependent function f(T) specified below. The present model for the updraft velocity is much simpler than that employed by Sud and Walker: the buoyancy force is integrated in the vertical and scaled by a tunable parameter.

Each plume modifies the environmental θ and q profiles. These modifications are felt by all subsequent plumes invoked during the call. In addition to the modification of the background thermodynamic state, the plumes detrain mass and condensate into the environment, so that net effects,

$$DM = \sum_{k} D_{k}$$
 and $DC = \sum_{k} D_{k} q_{cc,k}$,

are obtained. *DM* and *DC*, the mass and condensate effects respectively, are passed to PrognoCloud to serve as sources for anvil cloud fraction and anvil cloud condensate. A net profile of precipitating convective condensate,

$$P_{RAS} = \sum_{k} \delta q_{pc,k}$$
,

is also passed to PrognoCloud. Finally an estimate of updraft areal fractions is made using the total mass flux through each layer along with the local vertical velocity estimate.

2.2.1.2 Large-Scale Cloud Scheme

Source Terms for Cloud. As described earlier, the scheme distinguishes two types of cloud; that produced by detraining convection and that produced by large-scale condensation. The first type will be referred to as anvil cloud here and denoted by the subscript *an*. The second type, statistical or large-scale clouds, will be denoted by the subscript *ls*.

Anvil Cloud. Anvil cloud condensate $q_{c,an}$ and anvil cloud fraction f_{an} are updated straightforwardly using DM and DC from RAS:

$$\delta f_{an} = DM / \rho \Delta z$$
, $\delta q_{c,an} = DC / \rho \Delta z$.

Large-Scale Condensation. Condensation is based on a PDF of total water as in Smith (1990) or Rotstayn (1999). However, GEOS5_Moist uses a boxcar with a spread determined by the local saturation humidity, q_{sat} .

The current cloud scheme can be interpreted as a prognostic PDF scheme with a bi-modal structure as shown in Figure 2.2.2.

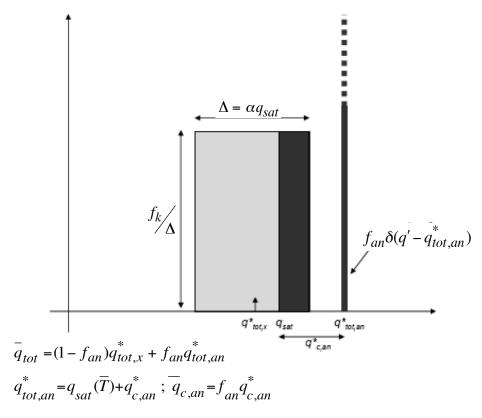


Figure 2.2.2: Schematic diagram of the implicit bi-modal PDF structure in the GEOS5_Moist cloud scheme. The current scheme consists of a boxcar PDF in non-anvil regions added to a δ -function containing contributions from detraining convection. In the symbols above, overbars refer to gridbox mean values.

Freezing and melting of cloud condensate

Fresh (new) cloud condensate is partitioned initially according to temperature using,

$$f_{ice}(T) = \begin{cases} 0 & T > T_{ice} \\ \left(\frac{T - T_{ice}}{T_{allice} - T_{ice}}\right)^4 & T_{ice} > T > T_{allice} \\ 1.0 & T < T_{allice} \end{cases}.$$

However, freezing progresses as long as the condensate remains in subfreezing temperatures. This freezing is parameterized as a temperature-dependent linear loss term for liquid condensate,

$$q_{l,\{ls,an\}FRZ} = -q_{l\{ls,an\}} \cdot \left(\frac{f_{ice}(T)}{\tau_{FRZ}}\right).$$

Whenever T exceeds T_{ice} melting of condensate is assumed to occur instantly and completely. For all calculations of saturation specific humidities a single ramped temperature-dependent saturation function is used.

2.2.1.3 Destruction of cloud

Destruction of cloud occurs in four ways: 1) evaporation "cloud munching"; 2) autoconversion of cloud condensate to precipitating condensate; 3) sedimentation of and 4) accretion of cloud condensate onto falling precipitation.

Evaporation cloud (E_c) "munching"

This mechanism is meant to represent destruction of cloud along edges in contact with cloud-free air. This process is parameterized using a microphysical expression from Del Genio et al. (1996),

$$E_c = -C_{E,c} \frac{1 - U}{\rho_w (A + B) r_c^2} q_c$$

where U is an environmental relative humidity, q_c is the cloud condensate mixing ratio, r_c is the cloud droplet radius derived from an assumed number density, A and B are temperature-dependent microphysical parameters. In GEOS-5 this loss is applied only to the anvil type.

Autoconversion of liquid and mixed phase cloud (A_c)

This is parameterized using the same Sundqvist-type formulation as used in the convective parameterization:

$$A_{c\{ls,an\}} = C_{0\{ls,an\}} f(T) \left\{ 1 - \exp\left(\frac{-q_{l,\{ls,an\}}^2}{q_{c,crit}^2 / f(T)^2}\right) \right\} q_{l,\{ls,an\}}.$$

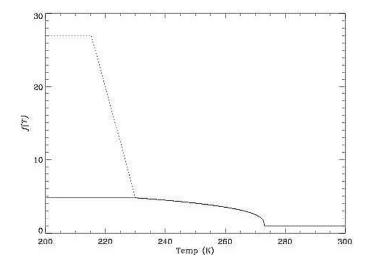


Figure 2.2.3: "Sundquist-factor" controlling low-temperature autoconversion.

The same temperature-dependent factor f(T) is used for ls and an clouds. The behavior of f(T) is shown in Figure 2.2.3. The increase below 273°K represents accelerated production of precipitation in mixed-phase clouds. The choice of this function is largely empirical. Destruction of cloud fraction by autoconversion is not considered.

Rapid conversion or fall out of frozen ice crystals is handled explicitly using the sedimentation formulation described next.

Sedimentation of ice cloud (S_c)

This is parameterized using cirrus ice fall speeds given by Lawrence and Crutzen (1998). However, instead using their regime division based on latitude, their expression for tropical cirrus is assigned to anvil clouds, and their mid-latitude form is assigned to large-scale clouds:

$$\begin{aligned} W_{F,i,an} &= 128.6 + 53.2 log_{10}(q_{c,i,an}) + 5.5 [log_{10}(q_{c,i,an})]^2 \\ W_{F,i,ls} &= 106 (q_{c,i,ls})^{0.16} \end{aligned}.$$

A simple one-way advection is used to represent the transition of ice cloud particles to sedimenting particles - the "fall through" approximation (e.g., Le Treut et al. 1994):

$$S_c = -C_{S\{ls,an\}} q_{i,\{ls,an\}} \frac{W_{F,i\{ls,an\}}}{\Delta z}$$

with empirically tuned parameters $C_{s\{ls,an\}}$. This approximation is known to overestimate production of frozen precipitation in other models (Rotstayn 1997).

Fall out and re-evaporation of precipitation and accretion of cloud condensate

All precipitation, including that produced within convective plumes, is finally disposed of in PrognoCloud. Three streams of precipitation, each with two phases, are considered: liquid and frozen precipitating condensate from ls clouds - $q_{p,l,ls}$; liquid and frozen precipitating condensate from an clouds - $q_{p,l,an}$, and liquid and frozen precipitating condensate from convective plumes (cu) - $q_{p,l,cu}$ $q_{p,l,cu}$.

The inputs to the subroutine are mixing ratios of precipitating condensate. The precipitating condensate in each stream and phase is accumulated from the top assuming complete fallout to obtain the downward flux of precipitation at level k, $P^{\downarrow}_{box}(k)$. To account for subgrid scale variability in precipitation this flux is scaled by a "shower area factor", A_s defined below, $P^{\downarrow}_s = P^{\downarrow}_{box} - A_x^{-1}$. This scaled flux is then used to estimate a typical drop size r_p using the Marshall-Palmer distribution. The quantity r_p is used to estimate precipitation fall velocities $W_{F,p}$ and ventilation factors Ve for the precipitation. These are now used along with the vertical thickness of layer k to estimate the fractional re-evaporation of precipitating condensate during its passage through the layer.

The shower area factor A_s is calculated slightly differently for convective and non-convective precipitation. For convective precipitation a weighted vertical mean of the updraft areal fraction is used. For non-convective precipitation, $q_{p,an}$ and $q_{p,ls}$, a similar weighted mean is calculated using the corresponding cloud fraction in place of updraft area fraction. The parameter E_f , the "exposed fraction", represents the fraction of precipitation exposed to grid box mean values of relative humidity, as opposed to the shielded fraction $S_f = 1$ - E_f which falls through a saturated cloudy environment (Figure 2.2.4). For nonconvective precipitation we assume $E_f = 1$. For convective precipitation a shear dependent exposure is assumed.

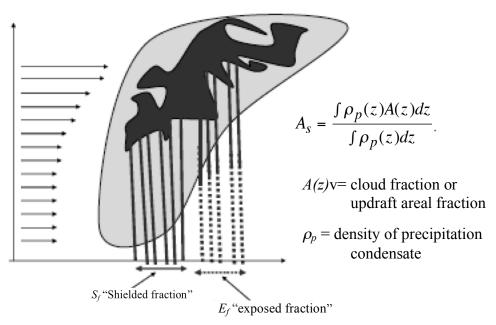


Figure 2.2.4: Schematic diagram of geometry assumed in rain re-evaporation calculation.

The change in precipitating condensate calculated within the re-evaporation subroutine is given by:

$$\delta q_p = -C_{E,p} V e \frac{1 - U}{\rho_w (A + B) r_p^2} q_p \left(\frac{\Delta z}{W_{F,p}} \right).$$

Accretion is parameterized simply using a Sundqvist-style expression as in Del Genio et al. (1996) or Sud and Walker (1999).

2.2.2 Radiation

The radiative transfer model used in GEOS-5 is one developed at the Goddard Climate and Radiation Branch. It has been integrated into various atmospheric models including the GEOS-5 AGCM, a mesoscale model, and a cloud ensemble model (Tao et al., 1996). The model is documented in Chou and Suarez (1999). It includes the absorption due to water vapor, O_3 , O_2 , CO_2 , clouds, and aerosols. Interactions among the absorption and scattering by clouds, aerosols, molecules (Rayleigh scattering), and the surface are fully taken into account. Fluxes are integrated over almost the entire spectrum, from 0.175 μ m to 10 μ m.

Depending upon the nature of absorption, different approaches are applied to different absorbers. In the ultraviolet (UV) and photosynthetically active radiation (PAR) region, the spectrum is divided into 8 bands, and single O_3 absorption coefficient and Rayleigh scattering coefficient are used for each band. In the infrared, the spectrum is divided into 3 bands, and the k-distribution method is applied. Ten absorption coefficients are used in each band. The flux reduction due to O_2 is derived from a simple function, while the flux reduction due to O_2 is derived from pre-computed tables.

Reflection and transmission of a cloud and aerosol-laden layer are computed using the δ -Eddington approximation. Fluxes are then computed using the two-stream adding approximation. For a cloud layer, the optical thickness is parameterized as a function of cloud water/ice amount and the effective particle size, whereas the single-scattering albedo and asymmetry factor are parameterized as a function of the effective particle size. The parameterizations are applied separately to water and ice particles. A

maximum-random approximation, a combination of maximum and random cloud overlapping schemes, is adopted for the overlapping of clouds at different heights. Aerosol optical properties are specified input parameters to the radiation model.

The surface albedo is an input parameter and is separately specified for the UV and PAR region and the infrared. It is also separately specified for direct and diffuse fluxes so that a set of four surface albedos must be specified as input to the radiation routine.

A special feature of this model is that absorption due to a number of minor absorption bands is included. Individually the absorption in those minor bands is small, but collectively the effect is large, $\sim 10\%$ of the atmospheric heating. Integrated over all spectral bands and all absorbers, the surface heating is computed accurately to within a few watts per meter squared of high spectral-resolution calculations, and the atmospheric heating rate between 0.01 hPa and the surface is accurate to within 5%.

2.2.3 Turbulent mixing

The free atmospheric turbulent diffusivities are based on the gradient Richardson number.

Two atmospheric boundary-layer turbulent mixing schemes are used. The Louis et al. (1982) scheme is used in stable situations with no or weakly-cooling planetary boundary layer (PBL) cloud. The Lock et al. (2000) scheme is used for unstable or cloud-topped PBLs. The latter scheme includes a representation of non-local mixing (driven by both surface fluxes and cloud-top processes) in unstable layers, either coupled to or decoupled from the surface, and an explicit entrainment parameterization. The scheme is formulated in the moist conserved variables θ_l , the liquid–frozen water potential temperature, and q_t , the specific total water content, so that it can treat both dry and cloudy layers. In GEOS-5, the scheme is extended so that unstable surface parcel calculations include moist heating and entrainment.

GEOS-5 incorporates two gravity wave drag parameterizations, an orographic gravity wave drag formulation based on McFarlane (1987), and a formulation for non-orographic waves based on Garcia and Boville (1994).

The mountain waves are forced by the sub-grid orographic variability, $h' = sqrt (avg([h-avg(h)]^2))$, where avg() denotes an average over the scale of gridbox. The terrain data, h(x,y), is from the GTOPO30 data (http://edc.usgs.gov/products/elevation/gtopo30/gtopo30.html), with a resolution of approximately 1 km. The smallest scales (<10km) are not used to force gravity waves, but enter into an orographic form drag used in the turbulence. The nominal gravity amplitude at the surface is given by MIN(h', U/N), where U is the surface wind speed and N is the low level stratification frequency.

The non-orographic waves, important in the stratosphere and mesosphere, are launched at 100 hPa. GEOS-5 uses an 8 wave-spectrum, with waves at phase speeds of 10, 20, 30 and 40 ms⁻¹ in both directions with respect to the wind at launch level. Their amplitude depends on their phase speed in a Gaussian way, $\sim \exp((-c/30.)^2)$. The amplitude is modified according to latitude, ranging from full amplitude in both polar regions (90-45 latitude bands) and dropping to 0.2 of the base amplitude in the tropics (20°S-20°N). The base amplitude, i.e., a wave with c approaching 0 near the poles, is $6.4e^{-3}$ N m⁻².

2.2.4 Chemical Species

2.2.4.1 The Ozone Model

Rather than transporting ozone (O₃), GEOS-5 GCM transports the odd-oxygen family: $Ox = O_3 + O(^3P) + O(^1D)$.

The chemical change in Ox is computed by

$$Ox(t + dt) = (Ox^* + P dt) / (1 + L dt),$$

where t is time, P is the Ox production rate, L is the Ox loss frequency, and Ox* is the intermediate Ox field that includes effects of transport and turbulent processes. Zonally invariant and monthly averaged coefficients P and L are used. They were generated by the Goddard two-dimensional chemistry and transport model, which employed surface source gas boundary conditions for the year 2000 (Fleming et al., 2001).

Ozone is derived from Ox. O_3 is specified to be equal to Ox for pressure higher than 1 hPa. At pressures lower than 1 hPa, O_3 is specified as equal to Ox during the nighttime and as

$$O_3 = Ox \exp[-1.5(\log_{10} p)^2],$$

in the daytime, where p is pressure in hPa. This relation is an empirical fit to equatorial daytime O_3/O_X ratios in a simulation that utilized a complete stratosphere-mesosphere chemistry mechanism. The diurnal ozone variation is due to fast ozone photolysis and subsequent recombination during nighttime in the mesosphere.

To avoid development of a low ozone bias in the upper stratosphere in GEOS-5, Ox production rates are adjusted following Stajner et al. (2004). The Ox production rates are modified so that the ozone chemical balance (which is P/L in the stratosphere) agrees with ozone climatologies from the Upper Atmosphere Research Satellite data (http://hyperion.gsfc.nasa.gov/Public/Analysis/UARS/urap/home.html) and SBUV data (Langematz 2000).

2.2.4.2 Other Constituents

The other radiatively active species, methane (CH₄), nitrous oxide (N₂O), chlorofluorocarbons (CFC-11, CFC-12), hydrochlorofluorocarbon (HCFC-22), and stratospheric water vapor (H₂O) are specified from the steady-state climatology of the Goddard two-dimensional chemistry and transport model, which employed surface source gas boundary conditions from 2000.

2.2.5 Surface processes

The surface exchange of heat, moisture and momentum between the atmosphere and land, ocean or sea ice surfaces are treated with a bulk exchange formulation based on Monin-Obukhov similarity theory. GEOS-5 employs a specified distribution of sea surface temperatures and sea ice, either from an observed weekly/monthly mean time series or annually repeating climatological mean. The sea ice distribution is prescribed.

2.2.6 The Catchment land surface model

GEOS-5 is coupled to a catchment-based hydrologic model (Koster et al., 2000) and a sophisticated multi-layer snow model (Stieglitz et al., 2001).

2.2.6.1 Overview

The one-dimensional "layered" framework used by traditional land surface models (LSMs) is arguably not amenable to an adequate treatment of runoff generation or subsurface soil moisture movement, since both processes in nature are largely controlled by spatial heterogeneity in soil moisture. The development of the GMAO Catchment LSM (Koster et al., 2000, Ducharne et al., 2000) is an attempt to improve

treatment of the subgrid horizontal structure of land surface hydrological processes. In this LSM, subgrid heterogeneity in surface moisture state is treated statistically, since computational constraints (now and in the foreseeable future) prevent its explicit resolution. Nevertheless, the applied distributions are related sensibly to the topography, which exerts a major control over much of the subgrid variability.

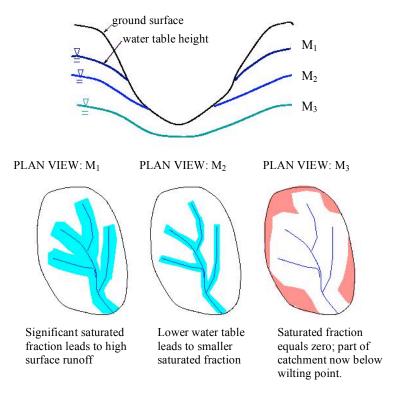


Figure 2.2.5: Separation of the catchment area into hydrological regimes.

2.2.6.2 Modeling Approach

The approach is illustrated in Figure 2.2.5, which shows three different levels of the (shallow) water table and the associated partitioning of the surface into three regions: (1) a saturated region, from which evaporation occurs with no water stress and over which rainfall is immediately converted to surface runoff, (2) a subsaturated region, from which transpiration occurs with limited water stress and over which rainwater infiltrates the soil, and (3) a "wilting" region, in which the water stress shuts down the transpiration completely. The relative areas of these regions, which vary in time, are unique functions of the local topography and the values of the Catchment LSM's three water prognostic variables. By continually partitioning the catchment into hydrologically distinct regimes and then applying different runoff and evaporation physics in the different regimes, the Catchment LSM should, at least in principle, produce a more realistic simulation of areally-averaged surface energy and water processes.

The soil water prognostic variables used by the Catchment LSM are "non-traditional" in that they are not strictly associated with soil layers. The main variable, the "catchment deficit", describes the equilibrium water table distribution and the associated distribution of the equilibrium soil moisture profiles in the overlying vadose zone. The second variable describes the degree to which the root zone is out of equilibrium with the catchment deficit, and the third describes the degree to which the near-surface moisture is out of equilibrium with the other two variables. The water transfer between the three variables and the baseflow flux out of the system are controlled in part by the local topography.

The model's other prognostic variables include an interception reservoir water content, a surface temperature, and the heat contents of six subsurface soil layers, from which time-varying vertical profiles of soil temperature over several meters can be derived. The model allows explicit vegetation control over the computed surface energy and water balances, with environmental stresses (high temperatures, dry soil, etc.) acting to increase canopy resistance and thus decrease transpiration. Six fundamentally different types of vegetation are considered in the current version of the Catchment LSM: broadleaf evergreen trees, broadleaf deciduous trees, needleleaf trees, grassland, shrubs, and tundra vegetation. Bare soil evaporation, transpiration, and interception loss occur in parallel. The energy balance formulations in the model (again, applied separately in each hydrological regime) were derived in large part from the Mosaic land surface model (Koster and Suarez, 1996), which in turn borrowed heavily from the SiB model of Sellers et al. (1986) for the transpiration calculation.

Snow is modeled using three prognostic variables (heat content, snow water equivalent, and snow depth) in each of three layers (Stieglitz et al., 2001). The melting and refreezing of snow, snow compaction, liquid water retention, and the impact of snow density on thermal conductivity and albedo are explicitly treated.

2.2.6.3 Implementation in GEOS-5

The Catchment LSM's implementation into the GEOS-5 system involves the "tiling" of a surface grid cell into a number of independent and irregularly shaped hydrological "catchment" elements. The catchment boundaries are derived from a 30-arc-second resolution (approximately 1 km) digital elevation model (DEM) provided by the U.S. Geological Survey. The delineation procedure considers network topology and drainage area (Verdin and Jenson, 1996; Verdin and Verdin, 1999) along with the application of ordering rules associated with a catchment coding system. For computational efficiency, and to take advantage of resolved heterogeneity in atmospheric forcing, catchments that straddle adjacent grid cells are separated into independent adjoining catchments, one in each grid cell. Runoffs produced by these artificially separated catchments can be combined into a single runoff that can then be routed across the continent.

Global distributions are needed for a number of model parameters. The global HYDRO1K dataset produced by the U.S. Geological Survey provided the distributions of compound topographic index needed to compute, within each catchment element, the parameters that control the shape of the shallow water table (using a TOPMODEL-type construct). Global soil texture information is derived from a 5-minute dataset assembled by Reynolds et al. (1999). Global seasonal climatologies of leaf area index and greenness fraction are taken from AVHRR-based data generated at the University of Wales and compiled by the Global Soil Wetness Project (Dirmeyer, 2006). Global distributions of vegetation type are taken from http://edcsns17.cr.usgs.gov/glcc/globdoc2_0.html, the Earth Resources Observation and Science website. GEOS-5 uses a two-stream approximation that lets snow-free albedo (for the visible and near-infrared bands) vary with solar incidence angle, but the values so produced are scaled so that they are consistent, on the monthly time scale, with the snow-free albedos produced by Moody et al. (2005) from MODIS data. Global surface emissivity data are taken from Wilbur et al. (1999).

2.2.6.4 Testing of the Catchment LSM

Various incarnations of the Catchment LSM have been evaluated extensively against observations through participation in the PILPS-2e project (Bowling et al., 2003), the Rhone-AGG project (Boone et al., 2006), and the second phase of the Global Soil Wetness Project (Dirmeyer et al., 2006). In addition, the Catchment LSM has proven to be an effective host for a soil moisture data assimilation system (Reichle and Koster, 2005, Reichle et al., 2006).

2.3 Specific Implementation for GEOS-5.0.1, GEOS-5.1.0, and GEOS-5.2.0.

The GCM used in GEOS-5.0.1 has a 0.5° latitude by 0.625° longitude horizontal resolution, with the prognostic variables discretized on a staggered D-grid (Figure 2.3.1). There are 72 vertical layers from the surface to 0.01 hPa. This system has an effective time step of 30 minutes, which is the time step of its physics parameterization (although the dynamics time step is considerably shorter). The primary variables are: wind components (u,v); scaled virtual potential temperature $(\theta^*=T_v/p^k)$; pressure thickness (of the Lagrangian control volume, p); and specific humidity (q).

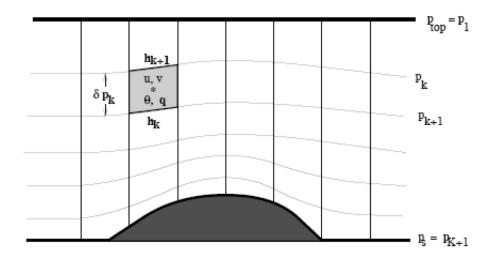


Figure 2.3.1 Lagrangian control volume and state variables for the GEOS-5 AGCM.

2.3.1 Ancillary initial and boundary data

A climatological aerosol distribution is used (Colarco et al., 2008). The model uses either a climatological ozone distribution or (in DAS mode) the ozone analysis generated from the DAS. The surface orography and its sub-grid scale standard deviation were derived from the 30-second US Geological Survey Global Topographic Data (GTOPO30). An area-preserving algorithm is used to map the high-resolution GTOPO30 dataset to model resolutions. The sea surface temperature and sea ice concentrations are derived from the weekly 1° Reynolds sea surface temperature (ERSST) version 2 (Reynolds et al. 2002). They are updated every time step using linear interpolation in time. GEOS-5 also employs an option to nudge the stratospheric water vapor to the zonal mean climatological HALOE (Halogen Occultation Experiment) and MLS (Microwave Limb Sounder) water vapor data (Randel et al. 1998).

2.3.2 The model grid

The GEOS-5 terrain-following lagrangian control volume (lcv) coordinates are similar to an eta coordinate system. The model output and many of the GEOS-5.0.1 products are lcv products. The products include the full three-dimensional pressure variables at both layer centers (PL_{ijl}) and layer edges (PLE_{ijl}). The pressures reported are on a hybrid-sigma coordinate. Indexing in the vertical starts at the top, i.e., lcv layer 1 is the layer at the top of the atmosphere, lcv layer 72 is adjacent to the earth's surface.

3. The GEOS-5 Analysis

At the heart of the DAS is the analysis itself. The analysis combines information from irregularly distributed observations with a model state in such a way as to minimize a specified cost function. The model state (also called the background) is obtained from a forecast initialized from a previous analysis. The weights assigned to each contribution to this combination depend on the specified error (or uncertainty) statistics for each of the observations and the model background. The GEOS-5 DAS uses the GSI analysis solver developed at NCEP. Other essential components are the quality-control software and the Radiative Transfer Model (RTM) needed for the radiance assimilation. The GSI is coupled to the Community Radiative Transfer Model (CRTM) developed through the JCSDA. For the stratospheric sounding unit (SSU) data used in MERRA, the GSI has been coupled to the GLATOVS RTM.

Some details of the GSI are presented in Section 3.1. The background (model forecast) error statistics are discussed in Section 3.2. The observation streams and their error characteristics are presented in Section 3.3. The RTMs are presented in Section 3.4. Information pertaining to the implementation of the analysis for versions 5.0.1 and 5.1.0/5.2.0 of GEOS-5 is given in section 3.2.5.

3.1 The GSI solver

The GSI solver was developed at NCEP to support their unified 3D-Var analysis system for global and regional models. The GSI builds upon the Spectral Statistical Interpolation (SSI) analysis which is documented at http://www.emc.ncep.noaa.gov/gmb/gdas/. The analysis variables are defined in grid space and recursive filters are the basic building blocks used to create background error covariance structures (Derber et al., 2003). The implementation uses the recursive filters to produce approximately Gaussian smoothing kernels and isotropic correlation functions (Wu et al., 2002). By superposition of Gaussian kernels with different length scales it is possible to generate non-Gaussian shapes, and generally to implement a large class of flow-dependent inhomogeneous background error covariance models (Purser et al., 2003a,b).

The variational analysis, x_a , is obtained by minimizing the scalar cost function

$$J(x) = (x - x_b)^T B^{-1}(x - x_b) + [y - h(x)]^T [E + F]^{-1} [y - h(x)] + J_C$$

with respect to the control vector, x. The background x_b represents a prior estimate of x and B is its expected error covariance. The vector y contains the available observations, the operator (also called the forward model) h(x) simulates these observations from x, and E+F=R contains the expected observation error covariances, including both instrument and representativeness errors. J_C represents additional constraints that can be imposed, such as mass-wind balance and moisture constraints.

The control vector or set of analysis variables, x, represents the atmospheric state at the central point in a 6-hour time window as well as predictor coefficients used for radiance bias correction (Derber and Wu, 1998; Dee, 2004, 2005) and surface temperatures used to correct model deficiencies at radiance data locations (Simmons, 2000). The forward model h(x) transforms the model variables into pseudo-observations. The value at the observation time is obtained by linear interpolation using background states provided at the analysis time and 3 hours before and after the analysis time. The forward model can be as simple as interpolation from model grid point to the observation location, or as complex as a radiative transfer model for satellite observations.

To accommodate nonlinear operators h (e.g., precipitation, wind speed, penalties on q for supersaturation and negative values), J(x) is minimized using an incremental strategy (Courtier et al., 1994) in which the problem is repeatedly linearized about an updated current solution (the *outer loop*). In the first outer loop iteration, the current solution is the 6-hour forecast. In later iterations, the current solution is the result from the previous iteration. Currently, only two outer loops are performed due to computational considerations.

A pre-conditioned conjugate gradient algorithm (the *inner loop*) is used to minimize the resulting quadratic cost function for the increments. The conjugate gradient algorithm requires the gradient of J with respect to the analysis variables. The gradient is evaluated using the adjoint of the transformation of the analysis variables into the observation variables.

The control variables, x, are:

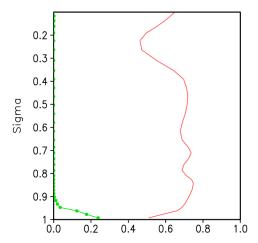
 ψ : stream function contribution to wind χ_{unbal} : unbalanced velocity potential function

 T_{unbal} : unbalanced temperature P_{unbal} : unbalanced surface pressure

q: moisture c_w : cloud water O_3 : ozone

and coefficients for the bias correction of the satellite radiance data.

The balanced part of the temperature is defined by $T_{bal} = G\psi$, where G is an empirical matrix that projects increments of stream function at one level to a vertical profile of the balanced part of the temperature increments. G is latitude dependent. The balanced part of the velocity potential is defined as $\chi_{bal} = c \psi$, where coefficient c is function of latitude and height. The explained variance for balanced temperature and velocity potential as a function of height at 60°N is shown in Figure 3.1.1. The balanced part of the surface pressure increment is defined as $P_{bal} = W \psi$, where the vector W integrates the appropriate contribution of the stream function from each level. The explained variance of the balanced surface pressure calculated in this manner is shown as a function of latitude in Figure 3.1.2.



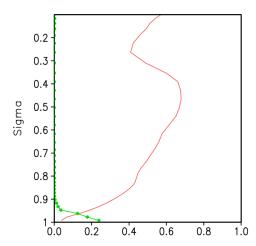


Figure 3.1.1: The explained variance of the balanced part of temperature (red curve) and velocity potential (green curve) at 60°N used in GEOS-5.0.1 (left) and GEOS-5.1.0 (right). The balanced velocity potential is largest at the surface to include a surface friction effect.

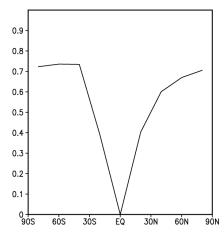


Figure 3.1.2: The explained variance of the balanced surface pressure as a function of latitude.

The updated (analyzed) fields are: zonal and meridional wind components (u, v), temperature (T), moisture (q), cloud water (c_w) , ozone (O_3) , surface pressure (p_s) , surface temperature (T_{skin}) . The analyzed wind components are calculated from the stream function and velocity potential.

3.2 The Treatment of Satellite Radiance Data

Satellite data have become an essential part of the observing system. They represent by far the largest volume of data ingested into operational NWP assimilation systems and their use in these systems has a measurable positive impact on forecast skill scores, especially in the Southern Hemisphere.

The analysis procedures for satellite radiance data are presented in Derber and Wu (1998) and McNally et al. (2000). As input to the surface emissivity calculation and the radiative transfer calculation of h(x), the background profiles of temperature, moisture (mixing ratio) and ozone (mixing ratio), and the surface temperature and 10m wind speed are interpolated to the observation location and the pressure levels used by the radiative transfer scheme. Based on this information and the surface type, the radiative transfer code generates a pseudo-observation of brightness temperature and the Jacobian matrix needed for the minimization.

3.2.1 Data thinning

The large volume of satellite data and the expense of including them in analyses forces a subsetting or thinning of these observations prior to assimilation. In addition, the errors implied by the combined observation and radiative-transfer error covariance matrix should be correlated both between adjacent observations and between channels of the same sounding. In practice, it is difficult to estimate these correlations; therefore, the observation errors are assumed to be un-correlated and this matrix is diagonal. In the GSI, the thinning strategy is defined by a specified resolution for each instrument type, the likelihood of the observation passing a quality control (QC) window check, the underlying surface properties, the difference between the observation time and the analysis time, and the distance between the observation location and the center of the analysis grid box. The size of the thinning box for each instrument type is summarized in Table 3.2.1.

Table 3.2.1: The sizes of the observation thinning box used in the GSI for different instrument types.

Instrument Type	AMSU-A	AMSU-B/MHS	HIRS/AIRS GOES Sounder/Imager	SSM/I	SSU
Thinning Box Size	145 km	240 km	180 km	160 km	200 km

3.2.2 Satellite data bias correction

Substantial biases are evident when satellite data are compared to the pseudo-observations derived from the background model [e.g., Eyre et al., 1993]. These biases may be due to bias in the background fields, or to errors in ground processing or in the forward processing (e.g., radiative transfer), residual contamination of the observations from cloud, instrument calibration errors, or inaccurate specification of instrument spectral response filters. Derber and Wu (1998) ascribe the dominant sources of these biases to ground processing errors and uncertainties in the radiative transfer calculation.

The biases vary spatially and depend on other satellite parameters such as the local zenith angle. For many channels, the mean value of the bias (calculated as the difference between the observed radiance (O) and that (F) calculated from the model background) is large relative to the instrument noise. It is therefore necessary to apply corrections either before the radiances are used in the assimilation or during the assimilation procedure. The latter approach, termed adaptive bias correction, has the advantage that the system automatically adjusts the bias estimate for the satellite data so as to maintain consistency with all available information, i.e., both the model background and all other observations. One of the disadvantages of this method is the possibility that the model bias will become incorporated in the coefficients and feed back into the system and amplify the model bias.

Dee (2005) describes the bias estimation procedure as follows. Bias parameters are estimated along with the model state in a variational analysis by augmenting the control vector with those bias parameters. To be explicit, the cost function of Section 3.1 can be written as

$$J(x) = (x - x_b)^T B^{-1}(x - x_b) + (\beta - \beta_b)^T B_{\beta}^{-1}(\beta - \beta_b) + [y - h(x) - b(x, \beta)]^T R^{-1}[y - h(x) - b(x, \beta)] + J_C.$$

The errors in the background estimate for the predictor coefficients, β_b , are generally correlated with the errors in the state estimate because they depend on the same data, however, because of lack of information, the cross-covariance in the GSI implementation is assumed to be zero giving the form of the cost function above.

The implementation in the GSI relies on linear predictor models so that the bias model included in the forward model is

$$b(\mathbf{x},\boldsymbol{\beta}) = \sum_{i=0}^{N_p} \beta_i \mathbf{p}_i(\mathbf{x}),$$

where b is the bias model and the p_i are the predictors. Only a few predictors are used in order not to overfit the biases, but the predictor coefficients for each channel and each sensor are allowed to be different. In the GSI, p_0 is a constant and the other predictors are: scan angle, lapse rate, lapse rate squared and (for microwave instruments) cloud liquid water. The predictors are scaled so that the same background error variance is used for each coefficient. A bias estimate is made for each scan position (for GOES it is for each integer local zenith angle). The total number of radiance bias parameters included in the system is roughly $N = N_p \times N_s \times N_c$, where N_p is the number of predictors used, N_s is the number of sensors being assimilated, and N_c is the number of channels per sensor.

The background estimate for β is the estimate obtained from the previous analysis. The bias estimates spin up to a stable estimate fairly quickly, viz., a few days. In GEOS-5, new satellite data are only introduced after a two-week passive assimilation used to estimate the bias parameters.

Figure 3.2.1a gives an example of the observation minus forecast calculation of the brightness temperature (i.e., O-F) for AIRS channel 1756 (wavenumber 1524.35cm⁻¹) without bias correction. This channel is sensitive to upper tropospheric humidity and the bias has large variation globally. The associated weighting function for this channel is also shown (Figure 3.2.1b). The bias in radiance data also varies with scan angle. The bias across scan angle is commonly detected in AMSU-A data. Figure 3.2.2 shows such bias for Channel 12 (57.3GHz) of AMSU-A on NOAA-15 and EOS/Aqua respectively.

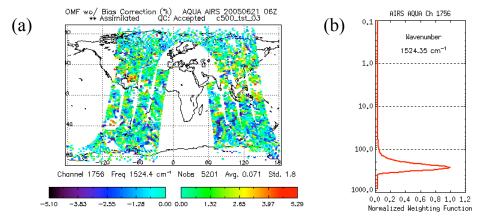


Figure 3.2.1: (a) The difference between the observed (without bias correction) and the calculated brightness temperature from the NWP model background (O-F), and (b) the normalized weighting function for AIRS moisture channel 1756.

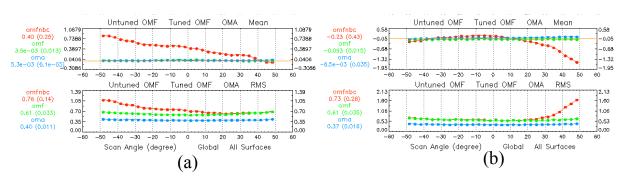


Figure 3.2.2 Examples of AMSU-A mean (upper panels) and standard deviation (lower panel)s of O-F values across the scan angles for (a) NOAA-15 and (b) Aqua. The red curve indicates O-F values before bias correction and the green curve shows O-F values after bias correction. The blue curve is the difference between observed and the calculated brightness temperature from the analysis.

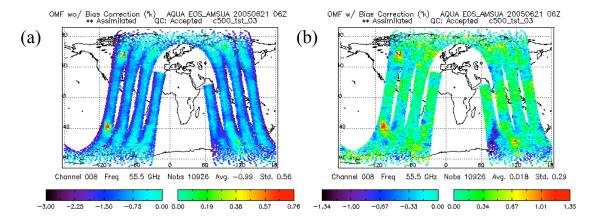


Figure 3.2.3: O-F maps for Aqua AMSU-A channel 8 data (a) before bias correction, and (b) after bias correction.

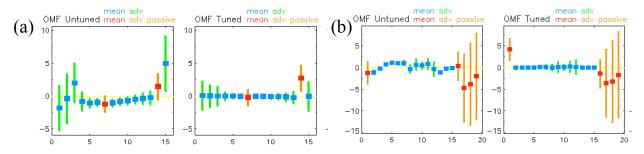


Figure 3.2.4: Global mean and standard deviation of O-F values before (left panels) and after (right panels) bias correction for each channel are shown for (a) Aqua AMSU-A and (b) NOAA-17 HIRS3.

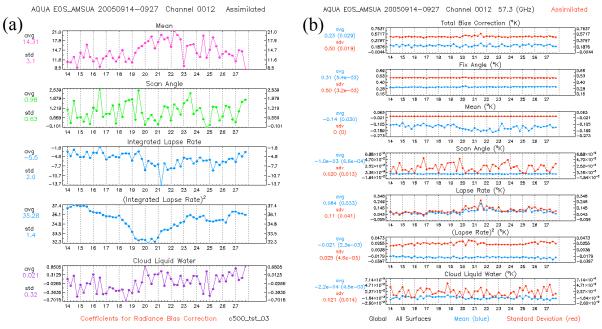


Figure 3.2.5: (a) Example of coefficients used in the variational bias correction and (b) the contributions to the bias correction for AQUA EOS AMSU-A channel 12.

Examples of the O-F values for channel 8 from EOS AMSU-A on board Aqua before and after the bias correction are show in Figure 3.2.3. Global averaged O-F value for each channel on EOS AMSU-A before and after the bias correction are shown in Figure 3.2.4. These examples indicate that the biases were eliminated by the variation bias correction scheme effectively. Any systematic components of the O-Fs that are not explained by these predictors are left in the data and are assumed to be systematic forecast model error. Examples of the bias correction coefficients for NOAA-15 AMSU-A channel 15 are shown in Figure 3.2.5a, and each term contributing to the bias correction in Figure 3.2.5b.

3.2.3 Ozone channels

AIRS ozone channels around 9.6 μ m are not actively assimilated. Increments to ozone from the assimilation of other radiance data are not used in GEOS-5. This choice was made to avoid systematic ozone analysis increments from radiance data that led to unrealistic ozone profiles in the polar night caused by accumulation of ozone in the lower stratosphere and excessive ozone reduction in the upper stratosphere. The impact of radiance data became more pronounced after the introduction of the IAU with its reduced noise in ozone transport. A part of the detrimental radiance impact on ozone is believed to be due to unmodeled polar stratospheric clouds (PSCs). The semitransparent PSCs are not represented in the GCM or in the forward model for the radiances. The cloud detection scheme does not exclude radiances affected by such thin clouds even though some radiances (such as AIRS "upper tropospheric moisture" channel at 6.79 μ m) are sensitive to ice PSCs (Stajner et al. 2007).

3.3 Other Assimilation Components

3.3.1 The Precipitation Assimilation

The assimilation system includes instantaneous rain rate estimates from SSM/I and the TRMM Microwave Imager (TMI). Details are provided in Treadon et al. (2002). The assimilated precipitation observation is $\ln(1+rain_rate)$. The forward model, h(x), is a simplified Arakawa-Schubert cumulus parameterization that includes cumulus momentum mixing and random selection of the convective cloud top from a range of values bounded by the sounding profile. The large scale precipitation model is based on Zhao and Carr (1997). Input to the forward model consists of surface pressure, temperature, specific humidity, cloud condensate (cwm), zonal wind, and meridional wind: $rain_rate_{tot} = rain_rate_{nv}(T,u,v,q,p_s) + rain_rate_{gs}(T,q,cwm,p_s)$. Only surface pressure is not included as a control variable in the tangent linear (TLM) and adjoint models. The simulated surface rain rates are most sensitive to the moisture and cloud condensate.

3.3.2 The Surface Temperature Analysis

Accurate specification of the (apparent) surface skin temperature is extremely important in the estimation of pseudo-observations of satellite brightness temperatures for channels which have a significant contribution from the surface. Hence this variable is included in the control vector, x. However, the resulting analysis is not used to update the skin temperature used by the forecast model. The rationale for this approach is provided by Derber and Wu (1998).

3.4 Specification of Background Error Statistics

A crucial part of the implementation of the any analysis is the specification of the background error covariance, B, and the observation error covariance, R. Each component of x has its own partition of the background error matrix B. The error statistics are estimated in grid space with the 'NMC' method

(Parrish and Derber, 1992; Rabier et al., 1998), i.e., by calculating the variances and covariances from the differences between 24-hour and 48-hour forecasts, forecasts initialized 24 hours apart, verifying at the same time.

3.4.1 State Variables

3.4.1.1 Stream function, u, v, humidity

The variance statistics of ψ are shown in Figure 3.4.1 as a function of latitude and sigma level. The error variance (m⁴ s⁻²) is larger in mid-latitudes than in the tropics and larger in the southern hemisphere than in the northern. The horizontal scales are larger in the tropics, and increase with height. The vertical scale factors are larger in the mid-latitude, and decrease with height. The vertical scale factors depicted in the figures below represent inputs to the recursive filters used to create the covariance functions. They are such that the vertical correlation generated from the recursive filter fits the scales estimated from the training data sets. The resulting vertical scale of the covariance function varies with height, becoming broader toward the top of the model. For example, see Figure 3.4.2 which shows the vertical correlation for pseudo-relative humidity at different levels, given a constant vertical scale factor of 1.0. The error variances and vertical scales for humidity are shown in Figure 3.4.3.

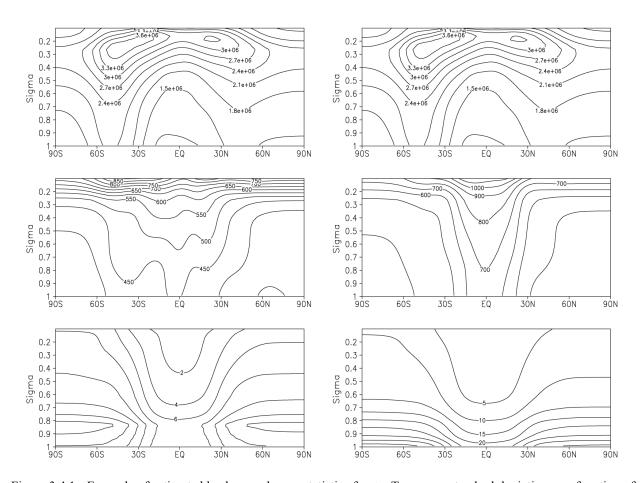


Figure 3.4.1: Example of estimated background error statistics for ψ . Top: error standard deviation as a function of latitude and sigma level (in m^2s^{-1}); middle: horizontal scales of covariance (in km); bottom: vertical scale factor of covariance. Left hand panels are the statistics used for GEOS-5.0.1; right-hand panels for GEOS-5.1.0.

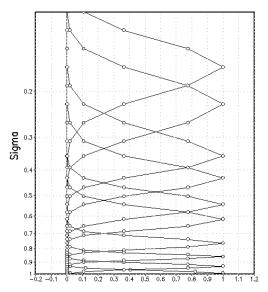


Figure 3.4.2: Example of the vertical correlation at different levels, given a constant vertical scale factor of 1.0. This structure is generated by the recursive filter to model the vertical correlation for all variables.

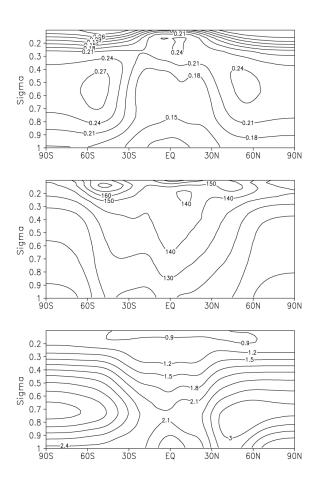


Figure 3.4.3: Example of estimated background error statistics for pseudo-relative humidity. Top: error standard deviation as a function of latitude and sigma level; middle: horizontal scales of covariance (in km); bottom: vertical scale factors for covariance.

Other elements of *B* can be seen through the marginal gain, i.e., the increment from a single observation, as shown in Figures 3.4.4 and 3.4.5.

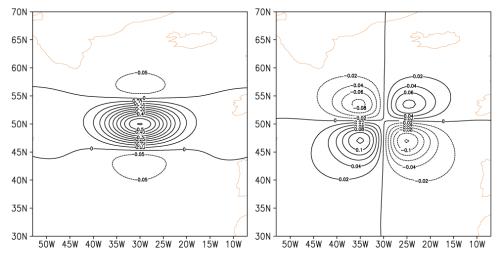


Figure 3.4.4: u (left) and v (right) increments $(x_a - x_b)$ at sigma level 0.267, of a 1 m/s westerly wind observational residual $(y_o - h(x_b))$ at 50°N and 330°E at 250 hPa.

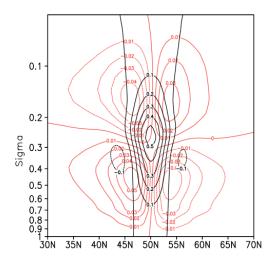


Figure 3.4.5: The vertical cross-section of u and T increments for the observation used for Figure 3.4.2.

3.4.1.2 Ozone

The background error for ozone is assumed independent from that for the other analysis variables. The background error standard deviation varies with model level: it is specified as ~4% of the global mean ozone on each level. The background error standard deviation is horizontally invariant. Horizontal background error correlations use length scales of ~400 km throughout troposphere and stratosphere, increasing to ~800 km at the top analysis level. Vertical correlations are specified using a common length scale of 0.8.

3.4.1.3 Satellite Bias Correction Coefficients

Since the satellite bias correction coefficients are analysis variables, it is necessary to specify the background error variances. These background error variances have been specified in a simple manner by scaling the predictors so that the variances of the various predictors are approximately equal (except the constant predictor) and then applying a constant diagonal matrix for the background errors. The constant used in the background errors gives fairly large weight to the values from the previous analysis.

3.4.2 The Mass-Wind Balance Constraint

The specification of the background error covariance matrix is extremely important in any data assimilation system since it is primarily the background error covariance matrix that determines the spreading of information from observations. Despite its importance, the way in which the background error covariance matrix is modeled in any practical assimilation system is dominated by the compromises that must be made in order to produce a viable computational algorithm.

Despite the advantages of the GSI in terms of the flexibility in representing the covariance structures, the modeling of the linear mass-wind balance through a linear balance constraint is not straightforward. In the GSI, to avoid the heavy computational burden of solving a Poisson equation at each assimilating level and at each iteration step, balance projections are introduced to link the balanced part of temperature and surface pressure directly with the stream function. The corresponding balance coefficients are estimated together with other background error statistics using the NMC method. This approach is indeed computationally-efficient, however, to ensure good wind-mass coupling, the balance coefficients have to be estimated in such a way to ensure the balanced geopotential height increments, which can be expressed from the balanced temperature and balanced surface pressure, are in good linear balance with the rotational wind increments from the GSI analysis. Otherwise, the balance projections will lead to inappropriate wind-mass coupling in which the information about the mass field will be extracted incorrectly from the wind observations, and *vice versa*.

Since the linear balance equation was not used in the tuning process for the original approach of estimating the balance coefficients, it was found that the resultant balance projections did not adequately model the linear wind-mass balance constraint. A new approach was developed that employs the linear balance equation and hydrostatic relationship to connect the balanced part of the temperature with the stream function, so that the covariance between the stream function and balanced temperature can be derived from the stream function related covariances. The balance coefficients estimated with this new approach ensure the wind-mass balance projections are equivalent to directly applying a linear balance constraint inside the GSI.

3.4.2.1 Linear Mass-Wind Balance Projections in the GSI

3.4.2.1.1 Wind-Mass Balance Projection Coefficients

The control variables of the GSI are stream function increments ($\delta\psi$), unbalanced velocity potential increments ($\delta\chi_{unbal}$), unbalanced virtual temperature increments (δT_{unbal}), unbalanced surface pressure increments (δP_{unbal}) and pseudo-relative humidity increments (δq). Typically the background error statistics for these control variables are estimated from a set of 24/48-hour forecast differences by the NMC method, and in the original implementation of the GSI the balance projection coefficients were estimated from the same set of forecast differences. The linear balance constraint to be satisfied so that the balanced geopotential heights are in good linear balance with the rotational winds is:

$$\nabla^2 \boldsymbol{\delta} \Phi = \nabla \cdot (f \nabla \boldsymbol{\delta} \boldsymbol{\psi}),$$

where f is the Coriolis parameter and $\delta\Phi$ is the geopotential height that can be expressed as

$$\delta\Phi = \int_{\sigma}^{1} R \delta T d \ln \sigma + \frac{RT_{s}}{p_{s}} \delta P$$
 (3.4.2.1)

from the integration over the hydrostatic equation in σ coordinates. In (3.5.2.1), R is the gas constant, p_s and T_s are standard surface pressure and surface temperature, respectively.

The balance projections are introduced in the GSI to avoid the time-consuming process of solving the linear balance equation directly. The projections define the balanced part of temperature (δT_{bal}) and surface pressure (δP_{bal}) directly from $\delta \psi$ by assuming

$$\delta T_{bal_k} = \sum_{l=1}^{N} v_{kl} \delta \psi_l,$$

$$\delta P_{bal} = \sum_{l=1}^{N} \mu_l \delta \psi_l,$$

where v_{kl} are the balance coefficients for δT_{bal} and μ_l the balance coefficients for δP_{bal} , and N is the number of assimilating levels. The vertical cross-covariance between the stream function at level m and temperature at level k can be constructed as

$$\langle \delta \psi_m, \delta T_k \rangle = \langle \delta \psi_m, \delta T_{bal_k} + \delta T_{unbal_k} \rangle.$$
 (3.4.2.2)

If we assume that there are no correlations between $\delta\psi$ and the unbalanced part of temperature, $\delta\Gamma_{unbal_k}$, then Equation (3.4.2.2) becomes

$$\langle \delta \psi_m, \delta T_k \rangle = \sum_{l=1}^N v_{kl} \langle \delta \psi_m, \delta \psi_l \rangle$$
 for $m = 1, ..., N$ and $k = 1, ..., N$.

Thus, we have the following linear system of equations for balanced temperature coefficients $\frac{1}{T}$

$$\boldsymbol{v}_{k} \equiv \left(\boldsymbol{v}_{k1}, \boldsymbol{v}_{k2}, \cdots, \boldsymbol{v}_{kN}\right)^{T}$$
:

$$\mathbf{C}_{\boldsymbol{\psi}}\boldsymbol{v}_{k} = \boldsymbol{\eta}_{k},\tag{3.4.2.3}$$

where $\mathbf{C}_{\psi} = (\langle \delta \psi_m, \delta \psi_l \rangle)$, l = 1, ..., N, m = 1, ..., N is the vertical covariance matrix of $\delta \psi$, and $\eta_k = (\langle \delta \psi_1, \delta \mathbf{T}_k \rangle, \langle \delta \psi_2, \delta \mathbf{T}_k \rangle, \cdots, \langle \delta \psi_N, \delta \mathbf{T}_k \rangle)^T$ the vertical cross-covariance vector between $\delta \psi$ and $\delta \mathbf{T}$. The matrix $(\mathbf{v}_k, k = 1, ..., N)$ forms an $N \times N$ coefficient matrix which is latitude dependent. Derived in the same way, the balance coefficients for surface pressure, $\boldsymbol{\mu} = (\boldsymbol{\mu}_1, \boldsymbol{\mu}_2, \cdots, \boldsymbol{\mu}_N)^T$, can be estimated from the following linear system of equations:

$$\mathbf{C}_{\psi}\boldsymbol{\mu} = \boldsymbol{\rho},\tag{3.4.2.4}$$

where $\rho = (\langle \delta \psi_1, \delta P \rangle, \langle \delta \psi_2, \delta P \rangle, \cdots, \langle \delta \psi_N, \delta P \rangle)^T$. The covariance matrix \mathbf{C}_{ψ} and vectors $\boldsymbol{\eta}_k$ and $\boldsymbol{\rho}$ are functions of latitude and are usually estimated by the NMC method. Practically, \mathbf{C}_{ψ} is a singular

matrix or a matrix very close to singular. Instead of solving Equation (3.4.2.3) or (3.4.2.4) directly, \boldsymbol{v}_k and $\boldsymbol{\mu}$ are estimated by finding the pseudo-inverse matrix $\mathbf{C}_{\boldsymbol{w}}^+$ of $\mathbf{C}_{\boldsymbol{w}}$.

3.4.2.1.2 Off-line background error covariance modeling

The relation between the mass and the wind through the wind-mass balance projections, are examined through L_{Φ} and R_{ψ} , the left-hand and right-hand sides of the linear balance equation, respectively:

$$\begin{split} L_{\Phi} &= \nabla^2 \delta \Phi, \\ R_{\psi} &= \nabla \cdot (f \nabla \delta \psi). \end{split}$$

Using the discrete form of (3.4.2.1), the covariance between $\delta \psi$ and L_{Φ} can be related to the balanced temperature and balanced surface pressure by

$$\left\langle \delta \psi_{m}, L_{\Phi_{k}} \right\rangle = -\sum_{n=1}^{k-1} \left(b_{nn} \left\langle \delta \psi_{m}, \nabla^{2} \delta \Gamma_{bal_{n}} \right\rangle + b_{nn+1} \left\langle \delta \psi_{m}, \nabla^{2} \delta \Gamma_{bal_{n+1}} \right\rangle \right) + \frac{RT_{s}}{p_{s}} \left\langle \delta \psi_{m}, \nabla^{2} \delta P_{bal} \right\rangle, \quad (3.4.2.5)$$

where $b_{nn} \equiv c_p(\tilde{\sigma}_{n+1} - \tilde{\sigma}_n)/2\tilde{\sigma}_n$, $b_{nn+1} \equiv c_p(\tilde{\sigma}_{n+1} - \tilde{\sigma}_n)/2\tilde{\sigma}_{n+1}$, $\tilde{\sigma} \equiv \sigma_n^{R/c_p}$, σ_n is the σ at the nth interface of the σ layers ($\sigma_1 = 1$), c_p is the specific heat at constant pressure. All the analysis variables are defined at the mid-point of each layer.

If we substitute the projections for δT_{bal_n} and δP_{bal} into (3.4.2.5), then we can see that the GSI representation of $\langle \delta \psi_m, L_{\Phi} \rangle$ depends on the mass-wind balance coefficients and the representation of $\langle \delta \psi, \nabla^2 \delta \psi \rangle$. Both $\langle \delta \psi, \nabla^2 \delta \psi \rangle$ and $\langle \delta \psi_m, R_{\psi} \rangle$ are the stream function related covariances that are modeled in the GSI by the recursive filters from the background error statistics for $\delta \psi$. If δT_{bal} and δP_{bal} satisfy the linear balance equation with $\delta \psi$, then we have

$$\left\langle \delta \psi_m, L_{\Phi_k} \right\rangle = \left\langle \delta \psi_m, R_{\psi_k} \right\rangle,$$
 (3.4.2.6)

and the balance projection scheme introduced in the GSI is equivalent to using the linear balance equation inside the analysis. It is very important that the balance coefficients be estimated in such a way to ensure (3.4.2.6) is satisfied in the analysis. Otherwise, the balance projections will provide the bad or even wrong wind-mass coupling in which the information about the mass field might be extracted incorrectly from the wind observations, and *vice versa*.

The linear mass-wind balance is a good first-order approximation in the wind-mass balance modeling, which can be examined by diagnosing $<\delta\psi_m,R_\psi>$ and $<\delta\psi_m,L_\Phi>$ directly from the same set of forecast differences (not shown).

3.4.2.1.3 The performance of the original GSI implementation

The wind-mass balance coefficients estimated with the current approach from equations (3.4.2.3) and (3.4.2.4) cannot ensure $<\delta\psi_m, L_{\Phi}>$ and $<\delta\psi_m, R_{\psi}>$ be close enough to have the correct wind-mass coupling in the analysis. Figure 3.4.5 shows the profiles of $<\delta\psi_m, R_{\psi}>$ (solid curves) and $<\delta\psi_m, L_{\Phi}>$ (dashed curves) using (3.4.2.5) from the stream function's background error statistics and the balance coefficients estimated with the original approach with m=23 (σ = 0.5) and at the selected latitudes. We can see that $<\delta\psi_m, L_{\Phi}>$ and $<\delta\psi_m, R_{\psi}>$ are quite different, especially in the tropics. In the mid- and high-latitudes and at the certain levels (for example, σ = 0.2), the difference is relatively small (not shown), However, it is typical that there are relatively large differences from 30°S to 30°N no matter

which levels are selected. These differences will surely cause incorrect wind-mass coupling in the GSI analysis. This was confirmed by looking at the analysis increments generated exclusively from the wind-mass balance projections. Plots of R_{ψ} and L_{Φ} and their ratio (not shown) indicated that the balance coefficients tuned with the original GSI implementation do not satisfy the linear balance constraint except in parts of the mid-latitude troposphere. The differences between R_{ψ} and L_{Φ} are relatively large in the region from 40°S to about 40°N and from 200 hPa to levels in the stratosphere.

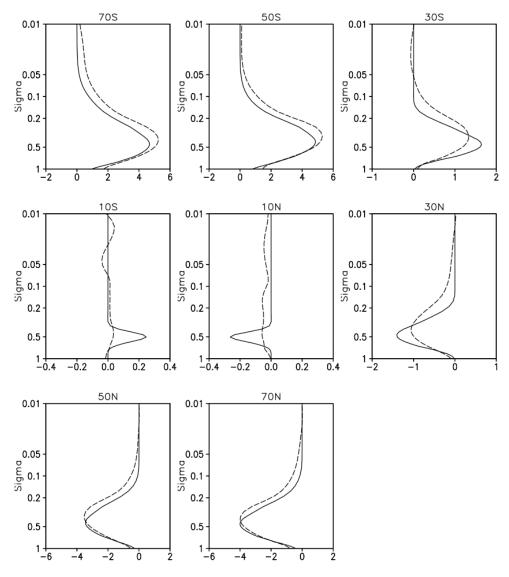


Figure 3.4.5: The profiles of $\langle \delta \psi, \nabla^2 \delta \Phi \rangle$ (dashed line) and $\langle \delta \psi, \nabla \cdot (f \nabla \delta \psi) \rangle$ (solid line) at eight selected latitudes with $\delta \psi$ being at $\sigma = 0.5$. These profiles are calculated from the balance projection coefficients estimated according to the original GSI implementation, and values have been multiplied by 10^3 .

3.4.2.2 A new approach for estimating the Linear Mass-Wind Balance Projections

A new estimation approach was developed which makes use of the linear balance constraint and the stream function related covariances to ensure that the wind-mass balance projections in the GSI satisfy the linear balance equation.

3.4.2.2.1 Formulation

From equation (3.4.2.5), we have

$$\left\langle \delta \psi_{m}, L_{\Phi_{k}} - L_{\Phi_{k+1}} \right\rangle = b_{kk} \left\langle \delta \psi_{m}, \nabla^{2} \delta \Gamma_{bal_{k}} \right\rangle + b_{kk+1} \left\langle \delta \psi_{m}, \nabla^{2} \delta \Gamma_{bal_{k+1}} \right\rangle, \tag{3.4.2.7}$$

where m=1,...,N and k=1,...,N-1. On the other hand, integration of (3.4.2.1) from the top ($\sigma=0$) to the bottom($\sigma=1$) leads to

$$\int_0^1 \delta \Phi d\sigma = \int_0^1 R \delta T d\sigma + \frac{RT_S}{\rho_S} \delta P.$$

Applying the ∇^2 operator to each term in the above equation and then discretizing yields

$$\sum_{j=1}^{N} L_{\Phi} \delta_{j} = R \sum_{j=1}^{N} \nabla^{2} \delta \Gamma_{j} \delta_{j} + \frac{R T_{s}}{p_{s}} \nabla^{2} \delta P,$$

where $\delta_i = \sigma_i - \sigma_{i+1}$. Constructing covariances using the above equation yields

$$\sum_{j=1}^{N} \left\langle \delta \psi_{m}, L_{\Phi_{j}} \right\rangle \delta_{j} = R \sum_{j=1}^{N} \left\langle \delta \psi_{m}, \nabla^{2} \delta T_{bal_{j}} \right\rangle \delta_{j} + \frac{RT_{s}}{p_{s}} \left\langle \delta \psi_{m}, \nabla^{2} \delta P_{bal} \right\rangle. \tag{3.4.2.8}$$

Equations (3.4.2.7) and (3.4.2.8) form a linear system with N equations but having N+1 unknown covariances $\langle \delta \psi_m, \nabla^2 \delta \Gamma_{bal_j} \rangle$ and $\langle \delta \psi_m, \nabla^2 \delta \Gamma_{bal_j} \rangle$. The linear system can be expressed as

$$\mathbf{B}\boldsymbol{\beta}_{m} = \mathbf{A}\boldsymbol{\alpha}_{m},\tag{3.4.2.9}$$

where

$$\boldsymbol{\alpha}_{m} = \left(\left\langle \boldsymbol{\psi}_{m}, \boldsymbol{L}_{\Phi_{1}} \right\rangle, \left\langle \boldsymbol{\psi}_{m}, \boldsymbol{L}_{\Phi_{2}} \right\rangle, \cdots, \left\langle \boldsymbol{\psi}_{m}, \boldsymbol{L}_{\Phi_{N}} \right\rangle\right)^{T},$$

$$\boldsymbol{\beta}_{m} = \left(\left\langle \boldsymbol{\psi}_{m}, \nabla^{2} \delta \boldsymbol{\Gamma}_{bal_{1}} \right\rangle, \left\langle \boldsymbol{\psi}_{m}, \nabla^{2} \delta \boldsymbol{\Gamma}_{bal_{2}} \right\rangle, \cdots, \left\langle \boldsymbol{\psi}_{m}, \nabla^{2} \delta \boldsymbol{\Gamma}_{bal_{N}} \right\rangle, \left\langle \boldsymbol{\psi}_{m}, \nabla^{2} \delta \boldsymbol{P}_{bal} \right\rangle\right)^{T},$$

$$\boldsymbol{A} = \begin{pmatrix} 1 & -1 & 0 & \cdots & 0 & 0 \\ 0 & 1 & -1 & \cdots & 0 & 0 \\ & & \ddots & & & \\ 0 & 0 & 0 & \cdots & 1 & -1 \\ \delta_{1} & \delta_{2} & \delta_{3} & \cdots & \delta_{N-1} & \delta_{N} \right)_{N \in \mathbb{N}},$$

and

$$\mathbf{B} = \begin{pmatrix} b_{11} & b_{12} & 0 & \cdots & 0 & 0 & 0 \\ 0 & b_{22} & b_{23} & \cdots & 0 & 0 & 0 \\ & & & \ddots & & & \\ 0 & 0 & 0 & \cdots & b_{(N-1)(N-1)} & b_{(N-1)N} & 0 \\ R\delta_1 & R\delta_2 & R\delta_3 & \cdots & R\delta_{N-1} & R\delta_N & \frac{RT_s}{p_s} \end{pmatrix}_{N\times(N+1)}.$$

A and **B** are constant matrixes depending on the layer structure of the vertical coordinate, the reference surface pressure and the reference temperature. The covariance vector α_m can be rewritten through the linear balance constraint (3.4.2.6) as

$$\alpha_{m} = \left(\left\langle \psi_{m}, R_{\psi_{1}} \right\rangle, \left\langle \psi_{m}, R_{\psi_{2}} \right\rangle, \cdots, \left\langle \psi_{m}, R_{\psi_{N}} \right\rangle \right)^{T},$$

which are stream function related covariances that can be estimated from the training data sets or replaced by their representation in the GSI through the recursive filters from the stream function's background error statistics. From **A**, **B** and α_m , the unknown vector β_m , which represents the covariance structures between the stream function and balanced part of temperature and surface pressure, can be estimated by

$$\beta_m = \mathbf{B}^+ \mathbf{A} \alpha_m, \tag{3.4.2.9}$$

where \mathbf{B}^+ represents the pseudo-inverse matrix of \mathbf{B} . One of differences between the new approach and the approach described in the section 3.4.2.1 is that η_k in (3.4.2.3) needs to be estimated independently from the training data sets, while in the new approach, $\boldsymbol{\beta}_m$ is derived from the stream function related covariances.

Once we have the covariances $\langle \delta \psi_m, \nabla^2 \delta \Gamma_{bal_k} \rangle$ and $\langle \delta \psi_m, \nabla^2 \delta P_{bal} \rangle$ for all m and k, the balanced temperature coefficients vector \mathbf{v}_k and surface pressure coefficients $\boldsymbol{\mu}$ can be estimated from the following linear equations:

$$\hat{\mathbf{C}}_{\psi} \mathbf{v}_{k} = \hat{\boldsymbol{\eta}}_{k},
\hat{\mathbf{C}}_{\psi} \boldsymbol{\mu} = \hat{\boldsymbol{\rho}},$$
(3.4.2.10)

which can be derived in the same way as the equations (3.4.2.3) and (3.4.2.4). $\hat{\mathbf{C}}_{\psi}$ is the $N \times N$ covariance matrix defined as $\langle \delta \psi_m, \nabla^2 \delta \psi_l \rangle$. It is another stream function related covariance matrix that needs to be estimated from the training data sets or approximated by the appropriate GSI representation. The vectors in the right sides of equations (3.4.2.10) are formed from the components of $\boldsymbol{\beta}_m$ in (3.4.2.9), that is,

$$\begin{split} \hat{\boldsymbol{\eta}}_{k} &= \left(\left\langle \delta \boldsymbol{\psi}_{1}, \nabla^{2} \delta \boldsymbol{T}_{bal_{k}} \right\rangle, \left\langle \delta \boldsymbol{\psi}_{2}, \nabla^{2} \delta \boldsymbol{T}_{bal_{k}} \right\rangle, \cdots, \left\langle \delta \boldsymbol{\psi}_{N}, \nabla^{2} \delta \boldsymbol{T}_{bal_{k}} \right\rangle \right)^{T} \text{ and } \\ \hat{\boldsymbol{\rho}} &= \left(\left\langle \delta \boldsymbol{\psi}_{1}, \nabla^{2} \delta \boldsymbol{P}_{bal} \right\rangle, \left\langle \delta \boldsymbol{\psi}_{2}, \nabla^{2} \delta \boldsymbol{P}_{bal} \right\rangle, \cdots, \left\langle \delta \boldsymbol{\psi}_{N}, \nabla^{2} \delta \boldsymbol{P}_{bal} \right\rangle \right)^{T}. \end{split}$$

3.4.2.2.2 Estimation of α_m and $\hat{\mathbf{C}}_w$

From the above formulations, it is clear that the wind-mass balance coefficients from the new estimation approach are dependent on two vertical covariance matrixes, i.e., $(\alpha_1, \alpha_2, ..., \alpha_N)$ and $\hat{\mathbf{C}}_{\psi}$. These two matrixes can be estimated either directly from the training data sets or indirectly from the stream function background error statistics through the GSI background error covariance modeling. The GSI

representations of α_m and $\hat{\mathbf{C}}_{\psi}$ are different from their direct diagnostics from the training data sets. The representation of vertical correlation for the stream function is a near-Gaussian function generated by two self-adjoint recursive filters, and the horizontal correlation is approximated by the superposition of three near-Gaussian kernels with different length scales. Compared with the corresponding direct diagnostics, the GSI representations are smooth and have no remote correlations.

To ensure the balance projection scheme is equivalent to using the linear balance constraint inside the GSI, α_m and $\hat{\mathbf{C}}_{\psi}$ should be estimated from the stream function background error statistics. If α_m and $\hat{\mathbf{C}}_{\psi}$ are estimated from the training data sets, then the estimated coefficients with the new approach will make the balanced geopotential height satisfy the linear balance equation with the diagnostic stream function error rather than the corresponding GSI representation since these two are quite different. So the estimation of these new balance coefficients involves the following steps: firstly, tuning the stream function background error statistics from the training data sets, then using an off-line code to calculate α_m and $\hat{\mathbf{C}}_{\psi}$ from those modeled stream function error statistics, and, finally, estimating the β_m , ν_k and μ from (3.4.2.9) and (3.4.2.10).

3.4.2.3 Evaluations of the New Wind-Mass Balance Projections

The wind-mass balance coefficients estimated with the new approach are different from those from the original approach described above. Since these coefficients have no clear physical meaning, we will instead compare the resultant balanced temperature and surface pressure. The vertical covariances for the balanced temperature and the surface temperature can be written as

$$\left\langle \delta \mathbf{T}_{bal_{k}}, \delta \mathbf{T}_{bal_{t}} \right\rangle = \mathbf{v}_{k}^{T} \mathbf{C}_{\psi} \mathbf{v}_{l},$$
$$\left\langle \delta \mathbf{P}_{bal}, \delta \mathbf{P}_{bal} \right\rangle = \boldsymbol{\mu}^{T} \mathbf{C}_{\psi} \boldsymbol{\mu}.$$

The vertical cross-covariance between these two balanced fields can be expressed as

$$\langle \delta \mathbf{P}_{bal}, \delta \mathbf{T}_{bal_k} \rangle = \boldsymbol{\mu}^T \mathbf{C}_{\psi} \boldsymbol{\nu}_l.$$

Since \mathbf{C}_{ψ} is an independent matrix, the differences in these covariances only reflect the differences in the balance coefficients. If we replace \mathbf{C}_{ψ} with its corresponding GSI modeling, then we have the GSI representation of these covariances.

Figure 3.4.6 shows the profiles of the standard deviation of the background balanced temperature error at selected latitudes used in GEOS-5.0.1 and 5.1.0. The resultant balanced temperature error in the upper levels is much smoother in either of the new balance projections (green curves) than in the original projections (red curves). In the tropics, the more balanced temperature can be explained from the stream function in the new projections. While in the original projection, the balanced temperature error at the high latitudes near $\sigma = 0.001$ is much larger in the southern hemisphere than in the northern hemisphere.

The GSI representation of vertical correlations from the original and the new balance projections are also quite different. Figure 3.4.7 shows the profiles of balanced temperature correlation at σ = 0.5 and at the same latitudes as Figure 3.4.6. With the new balance projections (green curves), the GSI representation of the correlation is much smoother and sharper especially at the low-latitudes, and has no remote correlation. The correlations resulting from the new balance projections have the typical two-sided negative lopes, which is different from those (red curves) from the original projections. The upper negative lobe in the extratropics is stronger than the lower negative lobe, however, if σ is at 0.2, the lower negative lobe is stronger than upper negative lobe, which can be seen in Figure 3.4.8. All of these are typical correlation features found in the temperature field. Figure 3.4.9 shows the profiles of the cross-correlations between the balanced temperature and balanced surface pressure. Again, the new cross-

correlation curves (green and yellow curves) are much smoother and retain the major features shown in the red curves.

The new wind-mass balance projections are equivalent to using the linear balance constraint inside the GSI. As in Figure 3.4.5, Figure 3.4.10 shows the profiles of covariances $<\delta\psi_m, L_{\Phi}>$ (dashed curves) and $<\delta\psi_m, R_{\psi}>$ (solid curves) with m=21 ($\sigma=0.5$), calculated based on the new balanced coefficients. Comparing Figure 3.4.10 with Figure 3.4.5, the differences between $<\delta\psi_m, L_{\Phi}>$ and $<\delta\psi_m, R_{\psi}>$ are reduced significantly. The slight differences, especially at the tropical latitudes, are due to poor conditioning of the matrix $\hat{\mathbf{C}}_{\psi}$ in which some of small singular values have to be removed before the estimation procedure. Figure 3.4.11 shows the zonal averages of absolute value of L_{Φ} (top panel) and R_{ψ} (middle panel) in the northern hemisphere, computed from the related analysis increments with the new wind-mass balance projections. The bottom panel shows that the balance constraint is satisfied over most of the globe. Although the ratio near the equator is slightly larger than 1, it is much reduced from the original implementation; and since the dominant error near the equator is unbalanced, the balance modeling near the equator is not a critical issue. The wind-mass balance from the new projections can also be seen in Figure 3.4.12, which shows the distribution of geopotential height and rotational wind increments. The rotational wind vectors follow the geopotential height lines, and the center of the mass matches the center of the wind very well.

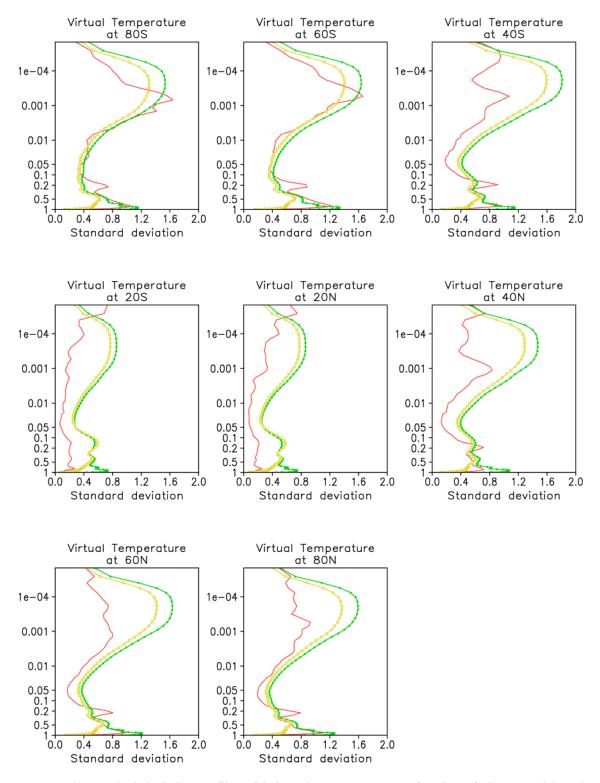


Figure 3.4.6: The standard deviation profiles of balanced temperature as a function of sigma at eight selected latitudes. The red curves are the estimates from the original GSI implementation, while the other curves are from the new approach. The green (yellow) curve shows the statistics used in GEOS-5.0.1 (GEOS-5.1.0).

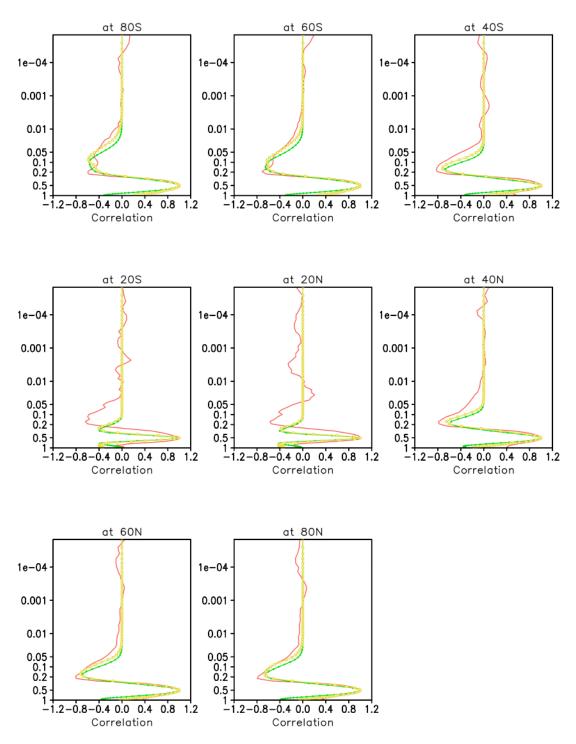


Figure 3.4.7: As in Figure 3.4.6, but for the correlation profiles at $\sigma = 0.5$.

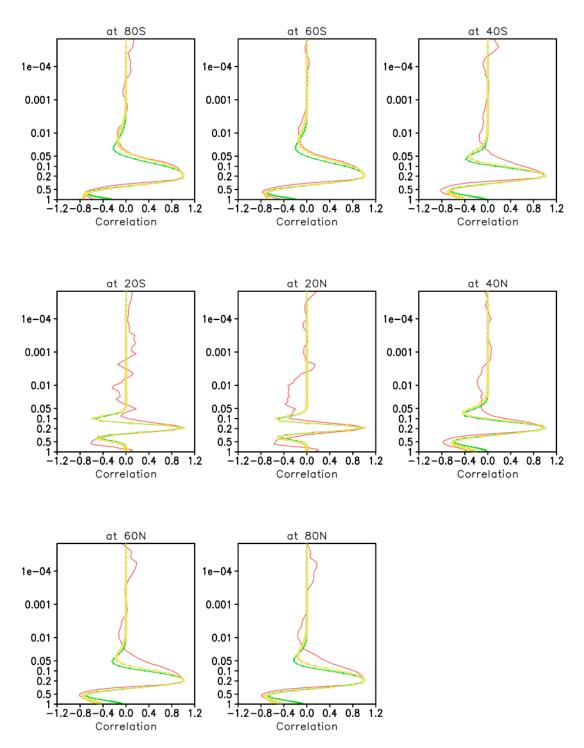


Figure 3.4.8: As in Figure 3.4.6, but for the correlation profiles at $\sigma = 0.2$.

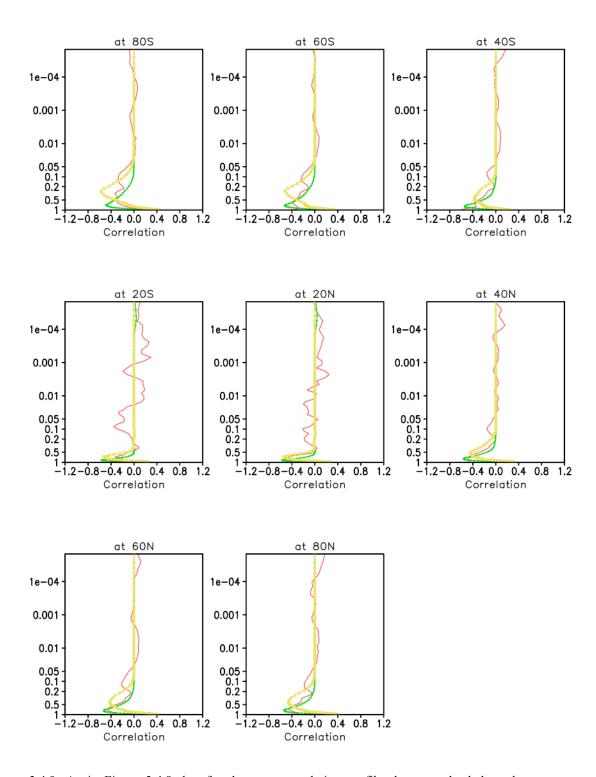


Figure 3.4.9: As in Figure 3.4.8, but for the cross-correlation profiles between the balanced temperature and balanced surface pressure.

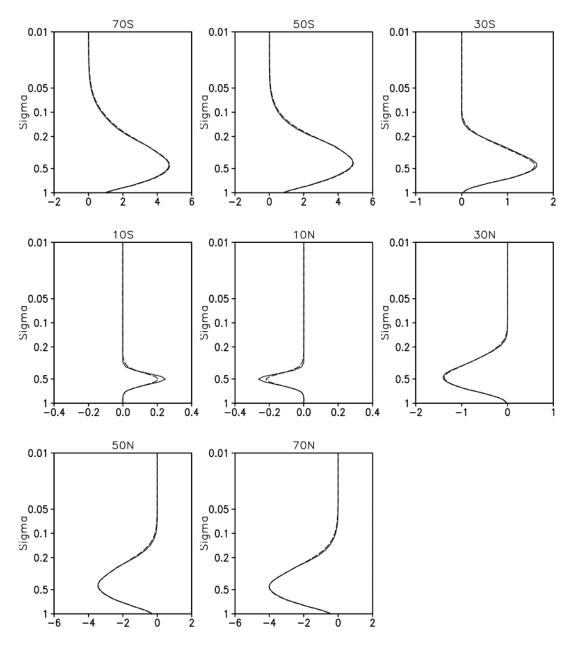


Figure 3.4.10a: As in Figure 3.4.5, but from the balanced projections estimated with the new approach used for GEOS.5.0.1.

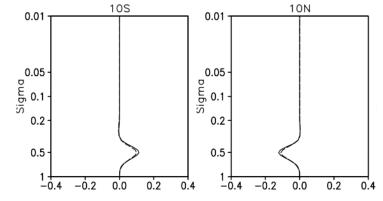


Figure 3.4.10b: As in Figure 3.4.10a, but for statistics used for GEOS.5.1.0 and only for 10°S and 10°N, there being little change at higher latitudes.

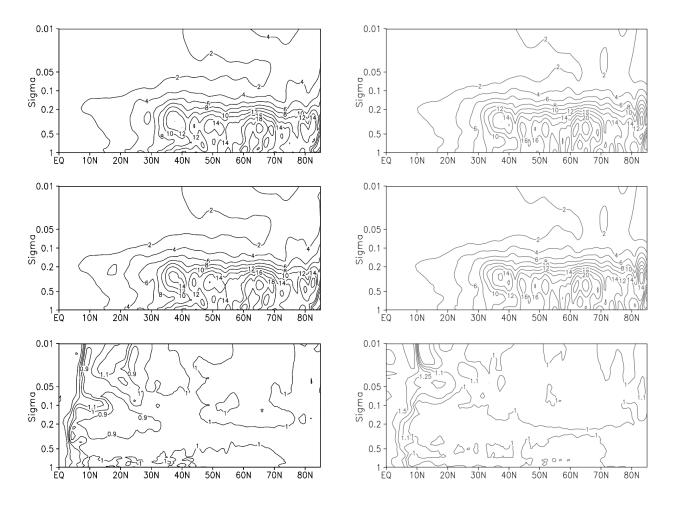


Figure 3.4.11: Zonal averages of $|L_{\Phi}| = |\nabla^2 \delta \Phi|$ (top), $|R_{\psi}| = |\nabla \cdot (f \nabla \delta \psi)|$ (middle). L_{Φ} and R_{ψ} are calculated based on the analysis increments which only includes the wind-mass balance projections with the new approach. All the values in the top and middle have been multiplied by 10^{10} . The bottom panel displays the ratio of top field to the middle, the contours of 0.5, 0.75, 0.9, 1.0, 1.1, 1.25, 1.5, 2.0, 4.0, 6.0 are plotted. Left hand panels are for GEOS-5.0.1; right hand panels are for GEOS-5.1.0.

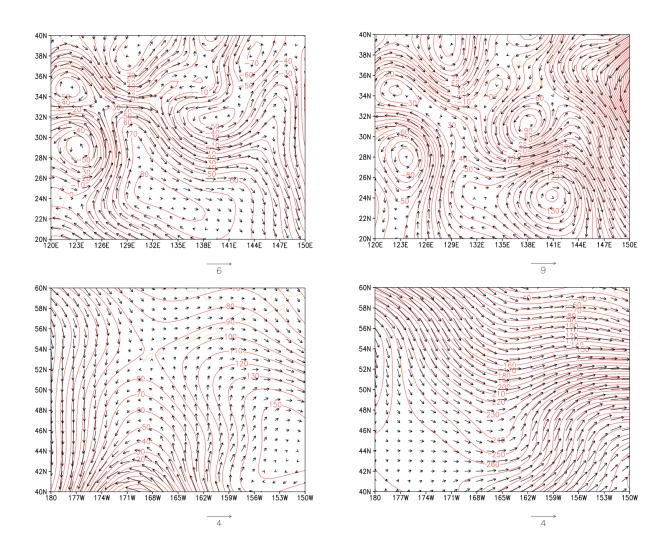


Figure 3.4.12: The distributions of geopotential height increments and vectors of the rotational wind from the windmass balanced projections estimated with the new approach with σ =0.5 (top) and σ =0.1 (bottom). The left-hand panels are for GEOS-5.0.1; right-hand panels for GEOS-5.1.0.

3.5 The Observing System and the Observation Error Statistics

The data streams currently assimilated by the GEOS-5 DAS are shown in Table 3.5.1. The observation error covariances are all univariate and the auto-covariance terms are delta-functions so that the corresponding entries in the matrix R are diagonal. Global constants (usually varying by level) for the observation error standard deviations used in GEOS-5 are given below in the discussion of each observation.

Table 3.5.1: Input observation data sources and parameters.

Conventional Data	
Radiosondes	u, v, T, q, P_s
PIBAL winds	u, v
Wind profiles	u, v
Conventional, ASDAR, and MDCRS aircraft reports	u, v, T
NEXRAD radar winds	u, v
Dropsondes	u, v, T, P _s
PAOB	P_{s}
GMS, Meteosat, cloud drift IR and visible winds	u, v
MODIS clear sky and water vapor winds	u, v
GOES cloud drift IR winds	u, v
GOES water vapor cloud top winds	u, v
Surface land observations	P _s
Surface ship and buoy observations	u, v, T, q, P_s
SSM/I	Rain rate, wind speed
TMI	Rain rate
QuikSCAT	u, v
Satellite Data	
TOVS 1b Radiances	AMSU-A: N15, N16, N18
10 V 5 To Teaching 5	AMSU-B: N15, N16, N17
	MHS: N18
	HIRS2: TIROS-N, N6, N7, N8, N9,
	N10, N11, N12, N14
	HIRS3: N16, N17
	HIRS4: N18
	MSU: TIROS-N, N6, N7, N8, N9,
	N10, N11, N12, N14
	SSU: TIROS-N, N6, N7, N8, N9,
	N10, N11, N14
EOS/Aqua Level 1b Radiances	AIRS (150 channels), AMSU-A
SSM/I radiances	DMSP-8, DMSP-10, DMSP-11,
	DMSP-13, DMSP-14, DMSP-15 (7
	channels)
GOES sounder T _B	GOES-08, GOES-10, GOES-12
	Channels 1-18
SBUV2 ozone (Version 8 retrievals)	Nimbus 7, NOAA 9, 11, 14, 16, 17

3.5.1 Conventional In-situ Upper-Air Data

3.5.1.1 Radiosondes, Dropsondes and Pibals

The predominant source of conventional upper-air data in GEOS-5 is radiosondes, which supply temperature, wind and moisture information at mandatory and "significant" levels. The temperature information is assimilated as virtual temperature by the GSI. While radiosonde data are quite valuable, providing profiles of mass and wind information, they are very anisotropically distributed, favoring land over ocean and the Northern Hemisphere over the Southern Hemisphere. There are also temporal variations in radiosonde soundings, with the majority of observations at 00 and 12 UTC; and only a few locations launching soundings at the other synoptic times.

The GEOS-4 system assimilated only radiosonde data at mandatory levels. The GEOS-5 analysis uses data from both mandatory and "significant" levels, however the observation error used is increased for profile observations closely spaced in the vertical.

The radiosonde network is augmented to a limited degree by dropsondes (from aircraft) and pilot balloons (which provide low-level wind profiles of lesser accuracy). Dropsondes are instrument packages similar to radiosondes that are dropped from aircraft. As with radiosondes, the dropsonde transmits information about temperature and humidity to the aircraft, and wind observations can be inferred from the horizontal motion of the dropsonde during its descent.

For pilot balloon (PIBAL) observations, a balloon inflated with either hydrogen or helium is tracked visually with an optical theodolite and the elevation and azimuth observations are used along with a predetermined ascent rate to calculate winds aloft. The NCEP processing also assigns the PIBAL report type to radiosonde wind reports that are not accompanied by a mass (height/temperature) report.

3.5.1.2 Aircraft Observations

Another significant source of conventional upper-air wind data are aircraft temperature and wind observations. These data are also highly anisotropic, and they have the additional characteristic of being primarily single level data. In the vicinity of airports, ascent and descent profile data are available. Humidity data is collected on a few flights but is not yet used in the assimilation system. Aircraft observations are obtained from manual (AIREP and PIREP) and automated (MDCRS and ASDAR) reports. The automated reports are more accurate and thus are assigned a smaller observation error.

3.5.1.3 Wind Profilers

Wind Profilers are vertically pointing clear-air Doppler radars that produce wind profiles in the vertical from measurements of energy backscattered by refractive index fluctuations that are advected by the wind (Hogg, *et al.*, 1983). The GSI currently assimilates wind profiler measurements from the NOAA Profiler Network (NPN) in the central U.S. and from a few other profiler sites (primarily in the tropical Pacific) that transmit PIBAL format wind reports over the GTS. Pacific stations have been reporting since about 1990, NPN since May 1992.

3.5.1.4 NEXRAD VAD Winds

Doppler radars measure mean radial velocity versus azimuth angle in 360 degree scans around the radar. Wind velocity and at various heights are derived from a best-fit sine wave to the radial wind components at given distances from the radar (Klazura and Imy, 1993). Hence, the observation represents the mean wind in a volume about the radar site. These observations are primarily low and mid-level winds and are generated at U.S. NEXRAD (WSR-88D) radar locations.

3.5.1.6 Synthetic (BOGUS) Tropical Cyclone winds

In the NCEP GDAS processing, if the tropical cyclone vortex relocation program encounters "weak" vortices which could not be used to update the global sigma first guess, the locations of these storms are passed to a subsequent program which then generates synthetic (bogus) wind mandatory level profile reports (throughout the depth of the storm) in the vicinity of the storm(s) to better define tropical systems for the analysis. The GEOS-5 system does not run the program that generates these synthetic wind profiles, but the synthetic observations will be assimilated if they are present in the operational PREPBUFR data received from NCEP.

Table 3.5.2: Observation errors for Radiosonde/Dropsonde 'mass' reports.

Pressure	Temper	rature (K)	Spec. Hun	nid. (g/kg)
(hPa)	Radiosonde	Dropsonde	Radiosonde	Dropsonde
> 1000	1.30	1.50	0.90	1.10
1000	1.10	1.30	0.80	1.00
950	0.90	1.10	0.80	1.00
900	0.70	0.90	0.80	1.00
850	0.60	0.80	1.00	1.20
800	0.60	0.80	1.10	1.30
750	0.60	0.80	1.30	1.40
700	0.60	0.80	1.30	1.50
650	0.55	0.75	1.30	1.50
600	0.50	0.70	1.30	1.50
550	0.50	0.70	1.30	1.50
500	0.50	0.70	1.30	1.50
450	0.50	0.70	1.30	1.50
400	0.50	0.70	1.30	1.50
350	0.55	0.75	1.30	1.50
300	0.65	0.85	1.30	1.50
250	1.10	1.30	_	_
200	1.20	1.50	_	_
150	1.20	1.50	_	_
100	1.20	1.50	_	_
75	1.20	1.50	_	_
50	1.20	1.50	_	_
40	1.40	_	_	_
30	1.60	_	_	_
20	1.85	_	_	_
10	2.00	_	_	_
5	2.00	_	_	_
4	2.00	_	_	_
3	2.00	_	_	_
2	2.00	_	_	_
1	2.00	_	_	_
< 1	2.50	_	_	_

Table 3.5.3: Observation errors for radiosonde, profiler and VAD wind (m/s).

Pressure				Profiler from		
(hPa)	Radiosonde	Pibal	Dropsonde	PIBAL rpt	NPN Profiler	VAD wind
> 1000	1.5	1.5	1.5	1.4	2.0	2.0
1000	1.5	1.5	1.5	1.4	2.0	2.0
950	1.5	1.5	1.5	1.5	2.0	2.0
900	1.5	1.5	1.5	1.5	2.0	2.0
850	1.5	1.5	1.5	1.5	2.0	2.0
800	1.5	1.5	1.5	1.6	2.0	2.0
750	1.6	1.6	1.6	1.6	2.0	2.0
700	1.7	1.7	1.7	1.6	2.0	2.0
650	1.8	1.8	1.8	1.8	2.0	2.0
600	1.9	1.9	1.9	1.9	2.0	2.0
550	2.0	2.0	2.0	2.0	2.0	2.0
500	2.1	2.1	2.1	2.1	2.1	2.1
450	2.2	2.2	2.2	2.3	2.3	2.3
400	2.2	2.2	2.2	2.6	2.6	2.6
350	2.3	2.3	2.3	2.8	2.8	2.8
300	2.3	2.3	2.3	3.0	3.0	3.0
250	2.4	2.4	2.4	3.2	3.2	3.2
200	2.4	2.4	2.4	2.7	2.7	2.7
150	2.4	2.4	2.4	2.4	2.4	2.4
100	2.4	2.4	2.4	2.4	2.1	2.1
75	2.4	2.4	2.4	2.4	2.1	2.1
50	2.4	2.4	2.4	2.4	2.1	2.1
40	2.4	2.4	2.4	2.4	2.1	2.1
30	2.5	2.5	2.5	2.4	2.1	2.1
20	2.7	2.7	2.7	2.4	2.1	2.1
10	2.9	2.9	2.9	2.4	2.1	2.1
5	3.1	3.1	3.1	2.5	2.1	2.1
4	3.3	3.3	3.3	2.6	2.1	2.1
3	3.5	3.5	3.5	2.7	2.1	2.1
2	3.7	3.7	3.7	2.8	2.1	2.1
1	3.9	3.9	3.9	2.9	2.1	2.1
< 1	4.1	4.1	4.1	3.0	2.1	2.1

Table 3.5.4: Observation errors for aircraft observations.

Pressure	Temperature (K)		Wind (m/s)			
(hPa)	AIREP	AMDAR	MDCRS	AIREP	AMDAR	MDCRS
> 1000	2.5	1.3	1.3	6.6	2.3	2.3
1000	2.5	1.3	1.3	6.6	2.3	2.3
950	2.3	1.2	1.2	6.6	2.3	2.3
900	2.1	1.1	1.1	6.6	2.3	2.3
850	1.9	0.9	0.9	6.6	2.4	2.4
800	1.7	0.9	0.9	6.6	2.4	2.4
750	1.5	0.9	0.9	6.1	2.4	2.4
700	1.3	0.9	0.9	5.6	2.4	2.4
650	1.2	0.8	0.8	5.1	2.4	2.4
600	1.2	0.8	0.8	4.6	2.4	2.4
550	1.2	0.8	0.8	4.1	2.5	2.5
500	1.2	0.8	0.8	3.6	2.5	2.5
450	1.2	0.8	0.8	3.6	2.5	2.5
400	1.2	0.7	0.7	3.6	2.5	2.5
350	1.2	0.8	0.8	3.6	2.5	2.5
300	1.3	0.8	0.8	3.6	2.5	2.5
250	1.3	0.8	0.8	3.6	3.0	3.0
200	1.3	0.9	0.9	3.6	3.0	3.0
150	1.4	0.9	0.9	3.6	3.0	3.0
100	1.7	0.9	0.9	3.6	3.0	3.0
75	1.7	1.0	1.0	3.6	3.0	3.0
50	_	1.0	1.0	3.6	3.0	3.0
40	_	1.0	1.0	3.6	3.0	3.0
30	_	1.1	1.1	3.6	3.0	3.0
20	_	1.1	1.1	3.6	3.0	3.0
10	_	1.0	1.0	3.6	3.0	3.0
5	_	1.0	1.0	3.6	3.0	3.0
4	_	1.0	1.0	_	3.0	3.0
3	_	1.0	1.0	_	3.0	3.0
2	_	1.0	1.0	_	3.0	3.0
1	_	1.0	1.0	_	3.0	3.0
	_			_		
< 1	_	1.0	1.0	_	3.0	3.0

3.5.2 Satellite Radiance Data

Remotely sensed information from satellites typically offers much greater and more isotropic coverage than that from conventional in situ sources. In contrast to GEOS-4, GEOS-5 primarily assimilates satellite level-1b (raw) radiances rather than retrievals. However, single level cloud motion vector winds obtained from geostationary satellite images, precipitation and surface wind speed estimates from microwave sensors, surface wind estimates from scatterometer radar, and column ozone obtained from the SBUV and SBUV/2 instruments are assimilated as retrievals.

For level-1b radiance data, the observation-minus-forecast departure statistics (both mean and standard deviation) provide an upper bound of the observation errors as they represent the summed contribution of errors in radiative transfer model, cloud detection, and errors in the background estimate of the atmospheric state. The fit of the GEOS-5 background profiles to the observed radiance for some instrument channels were found smaller than the current assigned values in GSI suggests that the weight currently give to these level-1b radiance data in GSI could be slightly increased. However, it is safer to be conservative and leave the observation error unchanged from the current assigned values. The assigned observation error variances in GSI for each instrument types are listed Appendix A.

3.5.2.1 TOVS/ATOVS

The TIROS Operational Vertical Sounder (TOVS) consists of three separate sounding instruments: the High-resolution Infrared Radiation Sounder 2 (HIRS2), later HIRS3 and HIRS4 for advanced TOVS (ATOVS); the Microwave Sounding Unit (MSU), later the Advanced Microwave Sounding Unit (AMSU), and the Microwave Humidity Sounder (MHS); the Stratospheric Sounding Unit (SSU), also replaced by AMSU. The TOVS instruments measure the radiance from Earth passively in different spectral regions specific to each type of remote sensing:

- in CO₂ or O₂ absorption zones to retrieve the vertical temperature profile,
- in water vapor or ozone absorption zones to determine the profiles and total concentrations of water or ozone
- in zones of low absorption to determine surface parameters.

The measured radiance includes thermal emission in the microwave and infrared channels and reflected solar radiation in the visible and shorter-wavelength infrared channels. Radiance is commonly expressed in terms of equivalent blackbody temperature (brightness temperature), as brightness temperature behaves more linearly with atmospheric temperature and other parameters than does the radiance.

TOVS has flown on the TIROS-N satellite and on NOAA operational polar-orbiting environmental satellites (POES) 6-12 and 14. NOAA 10 and 12 did not have an SSU instrument. The Advanced TOVS instrument (ATOVS), consisting of HIRS3 and AMSU, has been launched on the recent series of NOAA satellites; NOAA-15, 16 and 17, and HIRS4, AMSU-A and MHS on the latest, NOAA-18.

HIRS2 has has one visible channel (0.69 μm), seven shortwave IR channels (3.7 to 4.6 μm), and 12 longwave IR channels (6.5 to 15 μm). The nominal spatial resolution at nadir is 17.4 km. Details of the instrument and data can be found at http://www2.ncdc.noaa.gov/docs/podug/html/c4/sec4-1.htm. The HIRS/3 instrument has one visible channel (0.69 μm), seven shortwave IR channels (3.7 to 4.6 μm), and 12 longwave IR channels (6.5 to 15 μm). The nominal spatial resolution at nadir is 20.3 km in the visible and shortwave IR and 18.9 km in the longwave IR. The HIRS/3 instrument was flown on NOAA-KLM and instrument details are available at http://goespoes.gsfc.nasa.gov/poes/instruments/hirs3.html. HIRS/4 improves on the resolution of HIRS3, with a nominal spatial resolution of 10 km at nadir. Details of the instrument are available at http://goespoes.gsfc.nasa.gov/poes/instruments/hirs4.html.

MSU has 4 channels centered near the 57 GHz oxygen cluster. The nominal resolution is 110 km at nadir. Details of the instrument and data can be found at http://www2.ncdc.noaa.gov/docs/podug/html/c4/sec4-

3.htm. The AMSU-A measures scene radiance in the microwave spectrum. It is divided into two physically separate modules, each of which operates and interfaces with the spacecraft independently. Module A-1 contains 13 channels and Module A-2 contains two channels. AMSU-A1 consists of 12 V-band channels (3 through 14) and one W-band channel (15). AMSU-A2 contains the two lower frequencies (K-band channel 1 and Ka-band channel 2) The nominal resolution is 48 km at nadir. The AMSU-B is designed to allow the calculation of the vertical water vapor profiles from the Earth's surface to an altitude of about 200-mb pressure altitude. The highest channels: 18, 19 and 20, span the strongly opaque water vapor absorption line at 183 GHz and provide data on the atmosphere's humidity level. Channels 16 and 17, at 89 GHz and 150 GHz, respectively, enable deeper penetration through the atmosphere to the Earth's surface. The spatial resolution at nadir is nominally 16 km. Further details can be found at http://www2.ncdc.noaa.gov/docs/klm/index.htm.

The MHS is a five-channel microwave instrument intended primarily to measure profiles of atmospheric humidity. It is also sensitive to liquid water in clouds and measures cloud liquid water content. Because of the high variability of atmospheric water, the MHS has a higher resolution than the AMSU-A, with an nominal resolution of 16 km at nadir. MHS has four humidity channels in the 157 GHz to 190 GHz range. As with AMSU-A, it also has a surface-viewing window channel at 89 GHz, partly to ensure cross-registration of the two sounding instruments. Details of the instrument are available at http://goespoes.gsfc.nasa.gov/poes/instruments/mhs.html.

The stratospheric sounding unit (SSU) provided by the U.K. Meteorological Office were flown on several NOAA operational meteorological satellites. SSU employs the pressure modulation technique to measure stratospheric emission in 3 channels of the 15 μ m CO₂ band. The nominal resolution is 147 km at nadir. It is designed to retrieve temperatures in the stratosphere. The SSU has three channels with weighting functions which have peak response at pressure levels of 15, 6, and 2 mb respectively. Details of the instrument and data can be found at http://www2.ncdc.noaa.gov/docs/podug/html/c4/sec4-2.htm.

The TOVS/ATOVS observing system is summarized in Table 3.5.5.

Satellite Pre-launch ID Orbit Operational Data Coverage Instruments HIRS/2, MSU, SSU PM 1978/10/30 --- 1980/06/01 TIROS-N TN 1979/07/02 --- 1980/04/17 HIRS/2, MSU, SSU NOAA-06 NA AM 1985/04/08 --- 1986/11/17 NC HIRS/2, MSU, SSU 1981/07/11 --- 1985/02/19 NOAA-07 PM 1983/04/26 --- 1984/06/20 NE NOAA-08 HIRS/2, MSU, SSU AM1985/07/02 --- 1985/10/14 HIRS/2, MSU, SSU 1985/01/02 --- 1988/11/01 NOAA-09 NF PM 1986/11/25 --- 1991/09/01 NOAA-10 NG HIRS/2, MSU AM 1988/10/12 --- 1994/12/31 NOAA-11 NH HIRS/2, MSU, SSU PM 1997/07/15 --- 1999/02/25 1991/08/18 --- 1997/07/14 NOAA-12 ND HIRS/2, MSU AM1995/01/19 --- 2007/05/22 NOAA-14 NJ HIRS/2, MSU, SSU AM 1998/07/02 --- current date NOAA-15 NK HIRS/3, AMSU-A, AMSU-B AM 2001/01/01 --- current date NOAA-16 NL HIRS/3, AMSU-A, AMSU-B PM NOAA-17 HIRS/3, AMSU-A, AMSU-B AM 2002/07/15 --- current date NM HIRS/4, AMSU-A, HMS 2005/10/01 --- current date NOAA-18 NN PM

Table 3.5.5 Summary of TOVS/ATOVS observing system.

3.5.2.2 EOS/Aqua

The NASA EOS Aqua spacecraft was launched in May 2002. It carries a sounding suite consists of three instruments: the Atmospheric Infrared Sounder (AIRS), the Advanced Microwave Sounding Unit (AMSU) and the Humidity Sounder for Brazil (HSB). All three instruments are cross-track scanners.

AIRS, is a 2382-channel high-spectral-resolution grating spectrometer, with 2378 channels measuring infrared radiation from 3.7-15.4 μm and four visible channels and near-infrared radiation measuring from 0.4-0.94 μm. The primary purpose of AIRS instrument is to obtain atmospheric temperature and humidity profiles from the surface upward to an altitude of 40 km. Its infrared measurements have horizontal spatial resolutions of 13.5km at nadir, and its visible and near-infrared measurements have horizontal spatial resolutions of 2.3km at nadir. AIRS instrument is capable of providing high-resolution measurements in the vertical for 1-km layers in the troposphere and 3-5 km layers in the stratosphere. Details of the AIRS instrument can be found at http://aqua.nasa.gov/about/instrument airs.php.

AMSU, also referred to as AMSU-A on board of Aqua, is a 15-channel sounder consisting of two physically separate units AMSU-A1 and AMSU-A2. Module A1 unite contains 13 channels, and module A2 has 3 channels. Twelve of AMSU-A's channels measure radiation with frequencies between 50 and 60 GHz and are used predominantly for temperature sounding, whereas the other three channels measure radiation at frequencies of 23.8, 31.4, and 89 GHz are used predominantly for water vapor and precipitation measurements. The horizontal resolution of the AMSU-A data at nadir is 40.5 km, three times as coarse as the AIRS data. AMSU instrument is particular valuable in providing sounding information below clouds except for regions with heavy precipitation and optically thick clouds. Details of the AMSU-A instrument can be found at http://aqua.nasa.gov/about/instrument amsu.php.

HSB is a microwave humidity sounder. It has four channels, one measuring radiation at 150 GHz and the other three measuring at spectral bands centered on a strong water vapor absorption line at 183.31 GHz. HSB is particular important for allowing accurate humidity profiles to be obtained under overcast conditions. The horizontal resolution of HSB at nadir is 13.5km. Details of the HSB instrument can be found at http://aqua.nasa.gov/about/instrument hsb.php.

Details of the Aqua Project and related references can be found by navigating the website at http://aqua.nasa.gov/.

Level-1b radiances from AIRS and AMSU-A are used in GEOS-5. The full spectral resolution (2378 channels) AIRS data is too large for the global data assimilation model to digest the information. Therefore, a subset containing 281 channels from the original full spectral resolution set was selected for the NWP centers. This channel selection is listed in Appendix A. The observation errors assigned in the GSI for AIRS along with the instrument noise from the instrument team and their spectral locations are shown in Figure 3.5.1.

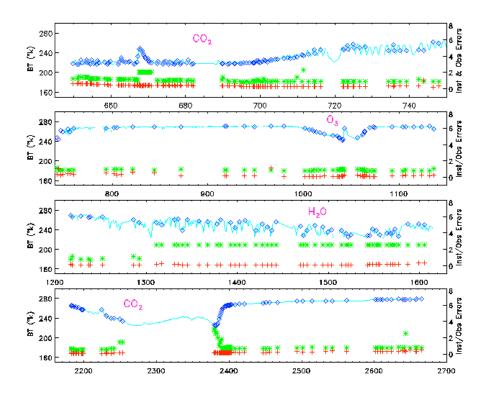


Figure 3.5.1 AIRS observed brightness temperatures for all 2378 channels are shown in light blue. The spectral location (blue diamond), instrument noise (red cross), and the assigned observation errors (green asterisk) in GSI for the 281-channel subset are also shown.

3.5.2.3 GOES Sounder Data

GOES satellites circle the Earth in a geosynchronous orbit. This allows continuous observation of the same region on earth. The geosynchronous plan is about 35800 km above the Earth, high enough to allow the satellites a full-disc view of the Earth. Normally, there are two GEOS satellites in operation. GOES-Ease is stationed at 75-West, and GOES-West is stationed at 135-West. They provide coverage of most of the Western Hemisphere. GOES satellites carry both sounder and imager. Currently, only GOES sounder data are used in GEOS-5 (Table 3.5.6). GOES sounder instrument has 18 thermal infrared bands plus a low-resolution visible band. The field of view is 8 km and is sampled every 10 km. The GOES sounder spectral selection is very similar to the HIRS instruments carried on the NOAA polar-orbiting satellites. It has six bands in the 15 micron band, two window channels, three mid-tropospheric water vapor bands, one ozone band, and five 4 near infrared band, and a visible band. Details of the instrument can be found at http://goespoes.gsfc.nasa.gov/goes/instruments/i m sounder.html.

Table 3.5.6 Summary of GOES satellite operation.

Satellite	Launch Date	Current Status
GOES-08 (I)	1994/04/13	Standard-by mode
GOES-10 (K)	1997/04/25	Operational GOES-West at 135°W
GOES-12 (M)	2001/06/23	Operational GOES-East at 75°W

3.5.2.4 SSM/I Radiances

The Special Sensor Microwave/Imager (SSM/I) is a passive microwave sensor on the Defense Meteorological Satellite Program (DMSP) satellite series. The instrument has seven microwave channels at 4 frequencies (19.35 GHz, 22.235 GHz, 37 GHz, and 85.5 GHz), each with dual (vertical and horizontal) polarization (except for the 22 GHz channel). This dual polarization allows the detection of surface properties. The SSM/I performs conical scans with a nominal earth incidence angle of 53.1 degrees and swath width of about 1400 km with footprint resolution of 40 km at a spacing of 25 km. The SSM/I radiance data used in GEOS-5 is summarized in Table 3.5.7. Additional information for the instrument is available at http://www.class.noaa.gov/release/data available/dmsp/index.htm.

Satellite	Operational Data Coverage
DMSP-08 (F08)	July 1987 December 1991
DMSP-10 (F10)	December 1990 November 1997
DMSP-11 (F11)	December 1991 May 2000
DMSP-13 (F13)	May 1995 Current
DMSP-14 (F14)	May 1997 Current
DMSP-15 (F15)	December 1999 August 2006

Table 3.5.7 Summary of DSMP satellite availability.

3.5.3 Satellite Retrievals

3.5.3.1 SBUV and SBUV/2

The Solar Backscatter Ultraviolet Instrument (SBUV) on Nimbus-7 and updated SBUV/2 instruments on NOAA POES series of satellites measure Solar irradiance and Earth radiance (from backscattered solar radiation) in the near ultraviolet spectrum. The measurements are taken from sun-synchronous orbits at nadir using 160 km wide field of view over the sunlit part of the Earth. Using ratios of backscattered radiances and Solar irradiances at 12 wavelengths total ozone columns and ozone profiles are retrieved. Version 6 retrievals (Bhartia et al 1996) were used in GEOS-5.0.1. Version 8 retrievals are used in GEOS-5.1.0 and GEOS-5.2.0. Version 8 retrievals (Bhartia et al., 2004) use a common set of *a priori* profiles from ozone climatology of McPeters et al. (2007) in order to remove any artificial trends due to *a priori*. Vertical resolution of Version 8 retrievals is 6-8 km in the upper stratosphere. Comparison of SBUV/2 Version 8 data with the Stratospheric Aerosol and Gas Experiment II (SAGE II) data show that most biases are within ±10%, except for larger negative biases near 50 hPa in the Tropics (Terao and Logan 2007). Version 8 data (available from http://disc.sci.gsfc.nasa.gov/data/datapool/TOMS/DVD-ROMS/) were provided to us by the Atmospheric Chemistry and Dynamics Branch at NASA/Goddard in order to include the latest calibration updates, extend NOAA-16 data to year 2005, and include NOAA-17 data from year 2006 onward.

Table 3.5.8: SBUV Observation errors.

	Layer bounds	
Level	(hPa)	Obs error (Du)
1	0.00-0.24	1.000
2	0.24-0.50	1.000
3	0.50-0.99	1.000
4	0.99-1.98	1.000
5	1.98-3.95	1.000
6	3.95-7.90	1.414
7	7.90-15.81	1.225
8	15.81-31.41	1.225
9	31.41-62.82	1.871
10	62.82-126.66	1.871
11	126.66-253.31	1.732
12	253.31-1013.24	1.414
Total		
ozone		2.236

3.5.3.2 Cloud track winds

Cloud track winds (CTW, also known as cloud-drift winds, as well as atmospheric motion vectors, AMV) are observations derived from sequences of images observed by satellites. The winds are calculated by an objective procedure that selects targets, assigns pressure altitude, and calculates atmospheric motion from the motion of the selected targets in successive images.

The GEOS-5 DAS uses cloud-track winds from geostationary satellites produced by NESDIS, JMA, and EUMETSAT; data from these sources provides near global coverage of AMV winds, equatorward of 60 degrees. CTW from MODIS on the EOS/Terra and Aqua platforms, also produced by NESDIS, provides data primarily in the polar regions.

Although the cloud track wind data are not thinned, the 'prepdata' processing at NCEP applies data selection based on the value of the quality index assigned to the wind by the data producer.

For NESDIS GOES hi-density winds, the quality marker (QM) is based on a recursive filter flag (RFF) value:

```
RFF <= 49 \qquad QM = 13 \text{ (exclude)} 
49 < RFF <= 55 \qquad QM = 3 \text{ (suspect - GSI inflates the observation error by a factor of 1.2)} 
55 < RFF <= 84 \qquad QM = 2 \text{ (normal)} 
RFF > 84 \qquad QM = 1 \text{ ('keep' flag, treat as normal)}.
```

For EUMETSAT BUFR winds, the QM is based on the quality indicator (QI) value, with the QI calculated using forecast background:

```
QI \le 0.8 QM = 13 (exclude)

QI > 0.8 QM = 2 (normal).
```

The EUMETSAT BUFR winds are produced every 90 minutes. The NCEP processing applies a time window so that only the one set of winds produced closest to the synoptic time is retained for use by the assimilation. The EUMETSAT ELW BUFR winds have been included in NCEP operational system since

24 April, 2001. Prior to that NCEP, processed 'SATOB' winds from the GTS and applied similar restrictions with respect to the quality indicator and time window.

The observation errors used in the GSI for cloud-tracked winds are provided in Table 3.5.9.

Table 3.5.9: Observation errors for cloud-tracked winds (m s⁻¹).

Pressure (hPa)	NESDIS picture triplet	NESDIS IR	NESDIS WV cloud top	JMA IR/VIS	EUMETSAT IR/VIS	MODIS IR	MODIS WV
1000	1.8	3.4	6.0	1.8	1.8	3.8	_
950	1.8	3.0	6.0	1.8	1.8	3.8	_
900	1.8	2.7	6.0	1.8	1.8	3.8	_
850	1.8	2.5	6.0	1.8	1.8	3.8	_
800	1.8	2.7	6.0	2.4	1.8	3.8	_
750	1.8	2.8	6.0	2.4	1.8	3.8	_
700	1.9	3.1	6.0	2.4	2.1	3.9	_
650	1.9	3.3	5.5	2.5	2.1	3.9	_
600	2.0	3.4	5.5	3.0	2.1	4.0	_
550	2.0	3.6	5.0	3.5	2.3	4.0	4.0
500	2.1	3.8	5.0	4.0	2.5	4.1	4.1
450	3.0	4.0	5.0	4.5	3.0	5.0	5.0
400	4.0	4.2	5.0	5.0	4.2	6.0	6.0
350	4.3	4.4	5.0	5.0	4.5	6.3	6.3
300	4.6	4.6	5.0	5.0	4.7	6.6	6.6
250	5.0	4.8	5.0	5.0	5.0	7.0	7.0
200	5.0	5.0	5.0	5.0	5.0	7.0	7.0
150	5.0	5.5	5.0	5.0	5.0	7.0	7.0
100	5.0	6.0	5.0	5.0	5.0	7.0	7.0
75	5.0	6.5	6.0	5.0	5.0	7.0	7.0
50	5.0	7.0	7.0	5.0	5.0	7.0	7.0

3.5.3.3 Precipitation estimates

1

SSM/I and TMI yield precipitation estimates over the oceans. These data are subsetted by generating a 1° grid of superobservations. The observational error variance is defined as $1.0 + 0.25 \times rain\ rate$.

3.5.3.4 Surface Wind Estimates

The NCEP GDAS operational processing takes SSM/I wind speed generated by the Neural Net 3 algorithm and superobs them onto a 1° latitude/longitude grid. The QuikSCAT scatterometer data are quality-controlled and then superobed onto a 0.5° grid.

For the MERRA system, Wentz SSM/I wind speed retrievals are superobed to a 0.5° latitude/longitude grid. The Quikscat scatterometer data for the MERRA system are processed as in the GEOS-4 system, selecting data only from the 'sweet spot' on each side of the swath and thinning by selecting winds from every other scan position.

The observation errors specified for surface winds varies according to the source:

SSM/I wind speed	2.0 m/s
QuikScat winds	2.5 m/s
ERS1/2 winds	2.5 m/s
Atlas buoy winds	2.2 m/s
Surface marine winds	2.5 m/s.

Surface marine observations are provided by ships and moored buoys.

3.5.4 Land Surface Observations

The GEOS-5 GSI assimilates surface pressure observations from land surface stations. For METAR observations without a surface pressure report, the altimeter setting is used to obtain a surface pressure value. Other land surface observations (temperature, moisture, wind) are kept as passive.

Table 3.5.10: Observation errors for surface pressure (hPa).

	Surface marine	Surface land	Dropsonde	METAR
> 1000	1.0	1.0	1.0	1.0
1000	1.0	1.0	1.0	1.0
950	1.0	1.0	1.0	1.0
900	1.0	1.0	1.0	1.0
850	1.0	1.0	1.0	1.0
800	1.0	1.0	1.0	1.0
750	1.0	1.0	1.3	1.3
700	1.1	1.0	1.6	1.6
650	1.2	1.2	_	_
600	1.2	1.2	_	_

Table 3.5.11: Observation errors for surface temperature and specific humidity.

	Temperature (K)		Specific Hum	idity (g/kg)
	Surface ship	Dropsonde	Surface ship	Dropsonde
> 1000	1.8	1.5	1.2	1.0
1000	1.8	1.5	1.2	1.0
950	1.8	1.5	1.2	1.0
900	1.8	1.5	1.2	1.0
850	1.8	1.5	1.2	1.0
800	1.8	1.5	1.2	1.0
750	2.0	1.5	1.5	1.0
700	2.3	1.5	1.5	1.0

3.5.5 Ocean Surface Observations

GEOS-5 assimilates surface pressure, temperature, moisture, and wind observations from ships and buoys. The GSI also uses sea surface temperature in the analysis. Surface marine observations are provided by ships, moored buoys, tide gauges and the Coastal-Marine Automated Network (C-MAN, see

http://www.ndbc.noaa.gov/cman.php).

The MERRA system includes PAOBs, which are synthetic surface pressure observations derived from manual analyses of surface pressure, produced by the Australian Bureau of Meteorology (Seaman and Hart, 2003).

3.6 Quality Control

The Quality Control (QC) procedures employed prior to assimilation are summarized at http://www.emc.ncep.noaa.gov/mmb/data_processing/data_processing/. Conventional data are QC'd by a sequence of programs prior to being passed to the analysis code. The Level 1b satellite radiance data from RTOVS (HIRS-2, MSU), ATOVS (HIRS-3, HIRS-4, AMSU-A, AMSU-B, MHS), and EOS/Aqua (AIRS, AMSU-A) as well as SBUV data are dumped into BUFR files and passed directly into the GSI which undertakes QC for the satellite data.

3.6.1 Conventional data

NCEP's CQCBUFR program is used to perform complex quality control on rawinsonde height and temperature data to identify or correct erroneous observations that arise from location, transcription or communications errors. The CQCBUFR includes a number of checks based upon differences from the background, including a hydrostatic check, an increment check, and horizontal and vertical interpolation checks and a lapse rate check. A baseline check is used to determine errors and/or changes in station location. The program also applies intersonde (radiation) corrections to the quality controlled rawinsonde height and temperature data. The degree of correction is a function of the rawinsonde instrument type, the sun angle and the vertical pressure level.

PROFCQC and CQCVAD programs perform complex quality control on wind profiler data and on NEXRAD or Vertical Azimuth Display (VAD) wind data from WSR-88D radars, respectively. The checks used are: increment, vertical statistical, temporal statistical, and combined vertical-temporal and are based upon differences from the background. The CQCVAD program includes an algorithm to account for the seasonal migration of birds.

The PREPACQC program performs quality control on conventional AIREP, PIREP and AMDAR (Aircraft Report, Pilot Report, Aircraft Meteorological Data Relay) aircraft wind and temperature data. The flight tracks are checked, with bad reports flagged and duplicate reports removed. AIREP and PIREP reports are further quality controlled by comparing isolated reports to the background and flagging outliers flagged and then inter-comparing groups of reports in close geographical proximity using both a vertical wind shear check and a temperature lapse check.

The ACARSQC program performs quality control on MDCRS and ACARS aircraft wind and temperature data. Currently only simple data bounds checks are performed.

The last program to execute QC before the data are passed to the GSI is OIQCBUFR. It performs an optimum interpolation based quality control on the complete set of observations in the PREPBUFR file. A number of independent checks (horizontal, vertical, geostrophic) are performed using all admitted observations. Each observation is subjected to the optimum interpolation formalism using all observations except itself in each check. A final quality decision (keep, toss, or reduced confidence weight) is made based on the results from all prior platform-specific quality checks and from any manual quality marks attached to the data.

For the GEOS-5 real-time forward processing system, the preprocessing QC is performed at NCEP prior to our receipt of the data. For the MERRA system, we conduct the preprocessing QC.

3.6.2 Satellite Radiance data

Quality control procedures depend on the observation type. They were briefly summarized by Derber (2005) at the 1st GSI user orientation. Presentation on the quality control of satellite radiance data can be found at http://www.emc.ncep.noaa.gov/gmb/treadon/gsi/documents/presentations/1st_gsi_orientation/.

HIRS, GOES, AIRS: High frequencies are eliminated during the day for reflected solar radiation contamination. Only cloud-free data are used. Screening is also conducted for the surface window to limit the magnitude of the necessary change in surface emissivity.

AMSU-A: Data are screened according to cloud liquid water, the scattering index, and on the magnitude of the necessary change in surface emissivity.

AMSU-B: Data are screened according to the ability to simulate quasi-window channels.

MSU: Data are screened according to the ability to simulate channel 1 (for channels 1 and 2).

GOES imager: Data are screened according to the clear sky fraction and the brightness temperature standard deviation.

SSM/I Radiances: Okamoto and Derber (2006) describe the methodology used for assimilation of SSM/I radiances in the GSI. SSM/I radiances are only assimilated over ocean; observations over land or ice are excluded. The QC of the SSM/I 1b radiances is based on the scattering index, si85, the difference between an estimate of the 85V brightness temperature from the other channels with the observed temperature (Ferraro, 1997). Over the ocean, the scattering index is:

```
si85 = [-174.4 + 0.715 \text{ Tb}19\text{V} + 2.439 \text{ Tb}22\text{V} - 0.00504 (\text{Tb}22\text{V})^2] - \text{Tb}85\text{V} and over the land:
```

 $si85 = [451.9 - 0.44 \text{ Tb}19\text{V} - 1.775 \text{ Tb}22\text{V} + 0.00574 (\text{Tb}22\text{V})^2] - \text{Tb}85\text{V}.$

Rain is detected if si85 > 10 and this information is used for data thinning and QC. Other checks are based on cloud liquid water (clw), a range check (70 < Tb < 320, for each channel), and a polarization check that (Vpol – Hpol) < -2 for each channel. The clw checks use a clw retrieval (after Weng, et al. 1997) from the 85 GHz channels as the first priority, from the 19 GHz channels as the next priority, and then from the 37 GHz channel if the others are not available. For example,

```
clw85 = -0.44 [log(290.-Tb85H) + 1.11 - 1.26 (log(290.-Tb22V)].
```

Cloud liquid water estimates are used in data selection/thinning when si85 is not available. The SSM/I radiances are also subject to a gross check on the observation increment, rejecting those with absolute value greater than $3\sigma_0$.

Common procedures: The quality control procedure common to all satellite data types is performed by a combination of two tests, a gross check and a check against the predicted values from nearby observations (a buddy check).

Gross check: For each observation location, an observation quality parameter is set based on the expected observational error variance for that channel. This quality control parameter is modified by the position across the track of the scan, whether it is over land, sea, snow, sea ice or a transition region, the elevation, the difference between the model and the real orography, and the latitude (the criterion is made tighter in the tropics). For the HIRS channels, the criterion is stricter if the observation is designated partly cloudy

by NESDIS, if the differences between selected window channel observations or the simulated window channels are too large, and for the shortwave channels if the solar zenith angle is small. Some of the modifications are designed to eliminate observations that are contaminated, and some to eliminate situations where the simulated observations are deficient. The observation quality parameter is then compared to the difference between the true and simulated observations. The observation is rejected if the difference from the simulated observation is greater than three times the observation quality parameter.

The buddy check: At the same time, the observation is compared to a simple interpolation of nearby observational increments to the observation location. The observation is if the difference from the simulated observation and the difference between the interpolated increments and the observation increment are both greater than the observation quality parameter. To minimize the number of observations that are rejected due to errors in nearby observations, the checking is repeated three times with only the observations that have passed the previous time through the quality control check being used for the interpolation of increments. This procedure allows the re-acceptance of some observations that were rejected in the previous passes through the data.

Note that the data rejections are performed independently for each channel. Thus, the rejection of one lower tropospheric HIRS channel because of possible cloud contamination does not necessarily result in the rejection of other tropospheric HIRS channels at the same location. This quality control procedure has some known deficiencies and probably rejects some good data in order to ensure the removal of all the bad data.

3.6.3 Precipitation Data

The quality control procedures for precipitation observations are outlined in Treadon et al. (2002). Because of the large boundary layer sensitivity of the convective scheme, a smoothness check is added to the data pre-processing. Those observations for which the vertical derivative of the sensitivity profile exceeds a given tolerance are not assimilated. The check flags about 5% of the SSM/I data and 4% of the TMI data.

A time screening is also applied to the observations. As the analysis relative time of the observation increases, the quality control error bounds smoothly decrease to zero. The quality control bounds also decrease to zero for observations poleward of 45° latitude. Observations are not used over snow-covered land, ice covered water, and poleward of 60° latitude. These surface type and latitude checks screen out 15.6% of the SSM/I data (0.6% for TMI). Finally, those observations which deviate from the background rain rate by more than three times the estimated observation error are not assimilated.

3.7 The Radiative Transfer Model

GEOS-5 versions to GEOS-5.2.0 uses the prototype version of the Community Radiative Transfer Model (pCRTM) for all satellite radiance data except for the historical SSU data stream input for MERRA. The GLATOVS radiative transfer model is used for the SSU.

The CRTM, developed under the auspices of the JCSDA, is integrated with the GSI. It is documented at http://www.orbit.nesdis.noaa.gov/smcd/spb/CRTM/ and in Han et al. (2006). The CRTM is comprised of various components involved in simulating satellite radiances. The four main components are:

- Atmospheric gaseous absorption
- Scattering and absorption by cloud and aerosols
- Surface optics emissivity and reflectivity
- The radiative transfer solution.

3.7.1.1 The gaseous absorption model

The operational gaseous absorption model used is Compact OPTRAN. The channel or spectral-response function convolved transmittance is modeled as

$$T_{ch} = T_{ch,w} T_{ch,o}^* T_{ch,d}^*$$

where $T_{ch,w}$ is the water vapor transmittance, and $T_{ch,o}^*$ and $T_{ch,d}^*$ are the effective transmittances of ozone and dry gas (McMillan et al., 1995), respectively. The transmittance component on the right hand side of the above equation is calculated as

$$T_{ch,g}(A_g) = \exp(-\int_{0}^{A_i} k_{ch,g}(A'_g) dA'_g),$$

where A_g is the integrated amount of water vapor, ozone, or dry gas, and $k_{ch,g}$ is the channel absorption coefficient of water vapor, ozone ,or dry gas. $k_{ch,g}$ is predicted as

$$\ln(k_{ch,g}(A_g)) = c_{g,0}(A_g) + \sum_{j=1}^{6} c_{g,j}(A_g) x_{g,j}(A_g);$$

$$c_{g,j}(A_g) = \sum_{n=0}^{N} a_{g,j,n} \ln(A_g)^n,$$

where the $x_{g,j}$ are predictors such as temperature and pressure and the $a_{g,j,n}$ are constants obtained through regression.

Minor gases that are generally well mixed such as CO₂, CO, N₂O, CH₄, CFCs, N₂, O₂, are not included as state variables but are fixed. Water vapor and ozone are generally not well-mixed and are included as variable gases.

3.7.1.2 The cloud absorption and scattering model

Currently, cloud and precipitation optical parameters are calculated with general Mie theory using a modified gamma distribution function. Several types of hydrometers including cloud ice, cloud liquid water, snow, graupel, hail and rain water are included. Parameters such as extinction coefficients, single scattering albedo and phase matrix elements are pre-calculated and stored in a lookup table (Liu et al., 2005). This table is searched with particle mean size and cloud water content.

Absorption and scattering by aerosols are under development.

3.7.1.3 Surface emissivity and reflectivity models

The CRTM employs a suite of microwave (MW) and infra-red (IR) surface emissivity and reflectivity models for land, ocean, ice and snow-covered surfaces.

Microwave:

- The MW *land emissivity model* (LandEM) computes land surface emissivity for various surface types, including snow, deserts and vegetation using the two-stream radiative approximation (Weng et al., 2001). The model takes satellite zenith angle, microwave frequency, soil moisture content, vegetation fraction, soil temperature, land surface temperature and snow depth as inputs and computes surface emissivity at vertical (V) and horizontal (H) polarizations.
- The empirical snow and ice emissivity models compute the emissivity via a combination of satellite window channel observations and emissivity databases collected from ground-based MW

instruments (Yan et al., 2004). The emissivity databases contain sets of emissivity spectral data measured at a zenith view angle of 50 degrees for various surface types. The window channel observations are used to identify the snow or ice surface type that best describes the surface condition observed by the window channels. After a spectrum is identified, it is adjusted for the requested zenith angle.

• The MW *emissivity over the ocean* surface is computed using FASTEM-1 (English and Hewison, 1998). It takes the satellite zenith angle, water temperature, surface wind speed, and frequency as model inputs and computes surface emissivity at V and H polarizations.

Infrared:

- Over the ocean the Infra-Red Sea surface Emissivity (IRSSE) model, as described in van Delst and Wu (2000), utilizes a lookup table of sea surface emissivities derived from the emissivity model for a wind-roughened sea surface (Wu and Smith, 1997). The lookup table variables are zenith angle (67 entries from nadir to 66.5°), frequency (153 entries from 600 to 3000cm⁻¹), and wind speed (23 entries from 0 to 15m/s). Linear interpolation is performed between the lookup table values.
- Over land surfaces, a look-up table is used for the 24 surface types in Table 3.8.1 using the emissivity database of Carter et al. (2002). The database contains surface reflectance measurements as a function of wavelength in both visible and IR spectral regions for these surface types. The emissivity is calculated from the reflectance under the assumption of a Lambertian surface in the IR spectral region.

Surface Type		
Compacted soil	Grass scrub	
Tilled soil	Oil grass	
Sand	Urban concrete	
Rock	Pine brush	
Irrigated low vegetation	Broadleaf brush	
Meadow grass	Wet soil	
Scrub	Scrub soil	
Broadleaf forest	Broadleaf(70)/Pine(30)	
Pine forest	Water	
Tundra	Old snow	
Grass soil	Fresh snow	
Broadleaf/Pine forest	New ice	

Table 3.7.1 Surface types included in the IR emissivity database.

3.7.1.4 The radiative transfer solver

The radiative transfer (RT) solver module solves the RT equation for given atmospheric optical depth profile, surface emissivity and reflectivity, cloud optical parameters and source functions. The clear and cloudy cases are treated with different methods, allowing a simple and efficient solution under the clear-sky condition. For cloudy cases, the radiative transfer is solved with the advanced doubling-adding method (Liu and Weng, 2006), in which fast algorithms are applied to compute layer source function and vertical radiative transfer integration.

The CRTM includes the forward and Jacobian models, as well as the Tangent-linear and Adjoint models. The forward model simulates satellite observed radiances. The Jacobian model computes radiance derivatives with respect to the input state variables.

3.8 Analysis Details for GEOS-5.0.1, GEOS-5.1.0, and GEOS-5.2.0

3.8.1 GEOS-5 analysis grid

In contrast to the Gaussian grid implementation at NCEP, the GEOS-5 analysis is conducted on the model's native grid, both horizontal and vertical.

3 8 2 Data Sources

The sources for the historical data streams for MERRA are given in the MERRA file specification document, available online at http://gmao.gsfc.nasa.gov/merra. The near-real-time GEOS-5 products and the corresponding historical product stream re-processed for the NASA instrument teams use the near-real-time streams utilized by NOAA/NCEP in their Global Data Assimilation System (GDAS). The exception to this is the SBUV version 8 stream used in GEOS-5.1.0. The historical stream is obtained from the Goddard Atmospheric Chemistry and Dynamics Branch. NCEP transitioned to the version 8 retrieval in January 2008. From that time, GEOS-5 has used the data stream from NCEP in forward processing.

3.8.3 Radiosonde Corrections for MERRA

The radiosonde temperature observations undergo up to three adjustments to remove or reduce biases. The first removes the unrealistically large 00/12 UTC time-mean temperature differences from NWS radiosonde observing stations that launch Vaisala RS-80 radiosondes. As shown in Redder et al. (2004), the differences, which occur primarily in the stratosphere, are a result of a coding error in the post-processing software at the observing stations. Software implementing the scheme to reverse this effect has been developed and applied offline to the dataset used for MERRA.

Second, the radiosonde temperature data at each station, worldwide, is adjusted using a text data file generated from the homogenization scheme (i.e. the removal of artificial changes in time-series) as described in Haimberger (2007a). This data file contains the temperature adjustments stratified by observing station, pressure level, synoptic hour (00 or 12 UTC) and detected artificial changes for the period from 1957 to 2006. The adjustments were generated using the dataset of Durre et al. (2006), that were re-corrected to reverse the effects of the software coding error at NWS stations as discussed previously (see Haimberger, 2007b).

Finally, the radiosonde temperatures are further adjusted to account for the effects of seasonal changes in the sun's elevation angle and, therefore, radiation bias of the thermistor. The annual average effects of the solar radiation are assumed to be implicitly accounted for in the adjustments generated by the homogenization scheme. The seasonal departures are estimated first by calculating the solar elevation angle at a given station location and observation time on the given date and on the date of the vernal (or autumnal) equinox. The radiation biases are then computed using the most recent version of the table generated at NCEP, and the difference is taken as an estimate of the seasonal departure.

Chapter 4 The GEOS-5 Data Assimilation System

4.1 Model – Analysis Interface

A number of steps is required to move between the state variables of the GEOS-5 GCM and the GEOS-5 analysis. Some are relatively minor, such as interpolating wind components back and forth from the GCM D-grid (Figure 4.1.1) to the analysis A-grid (essentially the " ϕ " points in Figure 4.1.1).

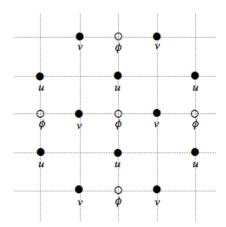


Figure 4.1.1: The D-grid layout in the GEOS-5 GCM; ϕ -points denote mass locations.

The major elements of the interface between the model and the analysis are:

- the use of an incremental analysis update method to apply the analysis;
- an after-analysis imposition of a constraint on the vertically-integrated divergence; and
- the calculation of a scaling factor to generate surface (2-meter, 10-meter) variables from the state variables in the model's lowest layer.

Although the GEOS-5 DAS uses the same effective grid for the model and the analysis, the grid employed for the analysis for the 1/2° system is slightly different from the model grid because of a recursive filter related constraint within the GSI for the number of grid-points to be a multiple of 8. Hence there is some additional interpolation required beyond the transform from D-grid to A-grid. The analysis itself is interpolated back to the native model grid prior to the calculation of the increments.

4.2 The Incremental Analysis Update (IAU)

To minimize the spurious periodic perturbations of the analysis, the DAS uses the Incremental Analysis Update (IAU) technique developed by Bloom et al. (1996). The IAU provides an effective filtering of the analysis increments found to be essential for the transport of ozone and trace gases within the GEOS-5 system. The implementation used for the GEOS-5 DAS is summarized in Figure 4.2.1. Every six hours, at the synoptic times, an analysis is performed using backgrounds at that time, three hours earlier, and three hours later, which incorporates observations during the six-hour period spanned by the three backgrounds. The results of this analysis are the products included in the two analysis collections. The analysis increments (i.e., the difference between the analysis and the corresponding synoptic background) are then divided by a time scale (in GEOS-5.0 and GEOS-5.1 the time scale is 6 hours) to produce an "analysis tendency." The model is then "backed-up", restarting it from its state three hours before the analysis time, and run for six hours, adding in the time-invariant "analysis tendency" in addition to its

normal physics tendencies. At that point a restart is created that will be used next time the model is backed-up, and the first background for the next analysis cycle is saved. This first 6-hour run is referred to as the "corrector" segment of the IAU. The run is then continued without an analysis tendency for another six hours, saving the other two backgrounds needed by the next analysis – one at the next synoptic time and another at the end of the six hours. This 6-hour run is referred to as the "predictor" segment of the IAU. The entire cycle is then repeated for subsequent synoptic times. Note that during each of the four daily analysis cycles the model is run for 12 hours.

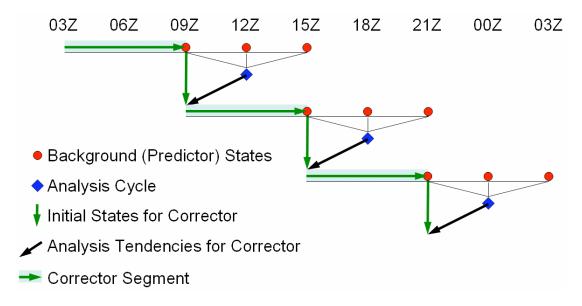


Figure 4.2.1: A schematic of the IAU implementation.

Except for the analyses themselves, all products from GEOS-5 are produced as model histories during the corrector run segment. The sequence of corrector segments (follow the green line in the figure) is a continuous model run, with the extra forcing term from the analysis tendencies. The analysis tendencies do change abruptly every six hours, but state variables are continuous (within the model's time step) solutions of the equations of motion, albeit with the extra forcing term.

4.3 Balancing Vertically Integrated Mass Divergence from Analysis Increments

At each analysis time the DAS produces both a *background* state and an *analysis* state of the prognostic wind v and pressure p fields. Defining the mass- or pressure-weighted variables

$$v^* = v\Delta p$$
$$D = \nabla \cdot v^*$$

where Δp is the pressure thickness of the model layer, we can define the analysis increment of massdivergence as

$$\Delta D = D_A - D_B.$$

Here the subscripts A and B refer to the analysis and background states, respectively.

The mass-divergence vertically integrated from the model surface to the model top is equal to the time

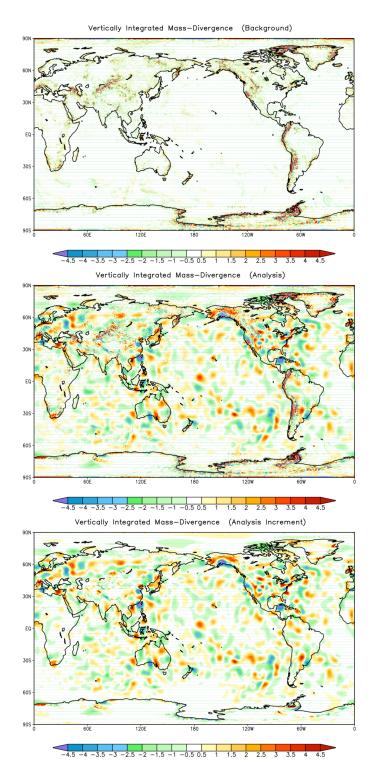


Figure 4.1: The vertically integrated mass-divergence (in arbitrary units) on 1 August, 2006 for the background (top), the analysis state (middle) and from the difference, or analysis increment (bottom).

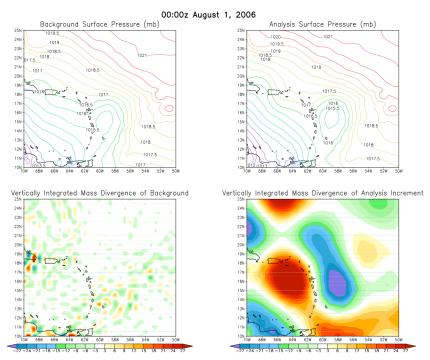


Figure 4.2 Initial condition of surface pressure for the background and analysis states. Also shown is the vertically integrated mass-divergence (arbitrary units) of the background and the (analysis-background) difference.

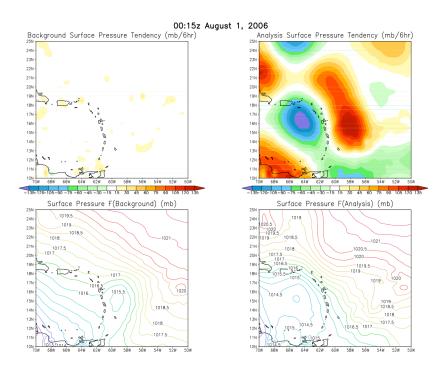


Figure 4.3 Initial surface pressure tendency of the background and analysis states, and the resulting surface pressure after 15 minutes of model integration.

tendency of the model's surface pressure. While the surface pressure time tendency of the background state is usually small (due to the inherent dynamical balancing properties of the model integration), the implied tendency from the analysis may be significantly large due to errors arising from uncertainties in the observations and error statistics as well as compromises made within the analysis algorithm.

In the vertically integrated mass-divergence for a typical background state, the largest tendencies occur near high topography, as expected, while the ocean values are quite small (Figure 4.1). The vertically integrated mass-divergence from the analysis state exhibits large coherent values covering the entire globe. These imbalances produce surface pressure tendencies on the order of 100 hPa per 6-hours in the first few timesteps, giving rise to large-scale pressure oscillations and wind adjustments.

Figure 4.2 shows the surface pressure for the background and analysis states, and the corresponding vertically integrated mass divergence for the area near Cuba and the Caribbean Islands on 1 August, 2006. Of particular interest is the low pressure center associated with Tropical Storm Chris. While the analysis was able to enhance and strengthen the initial condition associated with Chris, it left behind a state that contains very strong large-scale imbalances as evidenced by the vertically integrated mass divergence increment.

Figure 4.3 shows the surface pressure time tendency (calculated from the model's first time-step), in addition to the surface pressure after 15 minutes of model integration. The surface pressure time tendency is consistent with the vertically integrated mass divergence shown previously, and results in the low pressure center completely disappearing after the 15 minutes of integration. Thus, the analysis in this case produced an atmospheric state that was unsustainable by the model dynamics.

4.4.1 The Minimization Algorithm

To inhibit this computational adjustment due to the imbalances within the analysis state, we wish to find the smallest change to the analysis increment of mass-divergence (in a least-squares sense) such that the vertically integrated mass-divergence increment vanishes. In doing so, we will only make adjustments to the analysis wind field. Noting that:

$$\begin{split} \Delta D - \Delta D_o &= (D_A - D_B) - (D_{A_o} - D_B) \\ &= (D_A - D_{A_o}), \end{split}$$

where the subscript o refers to the initial guess, we may define the functional \mathcal{F} as

$$\mathcal{F} = \sum_{l=1}^{\text{LM}} \frac{1}{2} \left(\frac{D_{A_l} - D_{A_{ol}}}{\alpha} \right)^2 + \lambda \sum_{l=1}^{\text{NM}} (D_{A_1} - D_{B_l}).$$

Here $\left(\frac{D_{A_l} - D_{A_{ol}}}{\alpha}\right)$ is the penalty function of the analyzed mass-divergence that we want to minimize, λ is a

Lagrange multiplier used to enforce the strong constraint of vanishing vertically integrated massdivergence increment, LM is the total number of model levels, and α is an arbitrary scaling parameter. Taking the first variation of \mathcal{F} yields

$$\delta \mathcal{F} = \sum_{l=1}^{LM} \frac{1}{2} \left(\frac{D_{A_l} - D_{A_{ol}}}{\boldsymbol{\alpha}_l} \right) \frac{\delta D_A}{\boldsymbol{\alpha}_l} + \delta \boldsymbol{\lambda} \sum_{l=1}^{NM} (D_{A_1} - D_{B_l}) + \boldsymbol{\lambda} \sum_{l=1}^{NM} D_{A_1}$$

or, combining terms,

$$\delta \mathcal{F} = \sum_{l=1}^{LM} \frac{1}{2} \left(\frac{D_{A_l} - D_{A_{ol}}}{\alpha_l^2} + \lambda \right) \delta D_A + \delta \lambda \sum_{l=1}^{NM} (D_{A_1} - D_{B_l}).$$

Since δD_A and $\delta \lambda$ are arbitrary, minimization occurs when their coefficients are equal to zero:

$$\left(\frac{D_{A_l}-D_{A_{ol}}}{\alpha_l^2}+\lambda\right)=0,$$

and

$$\sum_{l=1}^{NM} (D_{A_1} - D_{B_l}) = 0.$$

Solving the above equations, we find:

$$\begin{split} D_{A} &= D_{A_{o}} - \lambda \alpha^{2}, \\ \lambda &= \frac{\sum D_{A_{o}} - \sum D_{B}}{\sum \alpha^{2}}. \end{split}$$

4.4.1.1 Case 1: $\alpha = 1$

With no scaling, the adjustment made is simply a constant applied uniformly in height:

$$D_{A} = D_{A_{o}} - \lambda,$$

$$\lambda = \frac{\sum D_{A_{o}} - \sum D_{B}}{\text{I M}}.$$

However, since adjustments will be made through the winds only, large wind changes are possible near the top of the model where the pressure thickness is very small.

4.4.1.2 Case 1:
$$\alpha = \Delta p$$

Here we normalize the penalty term by the pressure thickness, yielding:

$$\hat{D}_{A} = D_{A_o} - \lambda (\Delta p)^{2},$$

$$\lambda = \frac{\sum D_{A_o} - \sum D_{B}}{\sum (\Delta p)^{2}}.$$

We see that the adjustment is applied with a pressure scaling, resulting in small increments near the top of the model.

4.4.1.3 Case 1:
$$\alpha = D_{A_o} - D_B$$

Here we normalize the penalty term by the initial mass-divergence increment, yielding:

$$D_A = D_{A_o} - \lambda (D_{A_o} - D_B)^2,$$
$$\lambda = \frac{\sum D_{A_o} - \sum D_B}{\sum (D_{A_o} - D_B)^2}.$$

Here the magnitude of the adjustment is proportional to the local analysis increment of mass-divergence. Therefore, if the analysis made no local adjustment to the mass-divergence, the updated value will remain unchanged.

4.4.2 Wind Adjustment Algorithm

We may write the updated mass-divergence as:

$$D_A = D_A + \Delta D_A,$$

where, as shown above:

$$\Delta D_A = -\lambda \alpha^2.$$

Expressing the adjusted mass-divergence as an adjusted mass-weighted velocity potential:

$$\Delta D_{\scriptscriptstyle A} = \nabla^2 \Delta \chi^*,$$

we can then construct the adjusted mass-weighted divergent wind components as:

$$\Delta u_{\chi}^* = \frac{1}{a\cos\phi} \frac{\partial}{\partial\lambda} \Delta \chi^*,$$

$$\Delta v_{\chi}^* = \frac{1}{a} \frac{\partial}{\partial \phi} \Delta \chi^*.$$

These wind increments are then added to the original mass-weighted analysis winds, and subsequently descaled to arrive at the final winds produced by the balancing algorithm:

$$u_{final} = (u_A^* + \Delta u_{\chi}^*)/\Delta p_A,$$

$$v_{final} = (v_A^* + \Delta v_{\chi}^*)/\Delta p_A.$$

4.4.3 Results

In all cases (1, 2, and 3) the vertically integrated increment of mass divergence is forced to vanish (within truncation). Figure 4.4 illustrates this where we compare the zonal mean of the absolute value of the vertically integrated mass divergence increment from the standard analysis with the corresponding analysis after balancing (Case 3). Case 1 and Case 2 show nearly identical results.

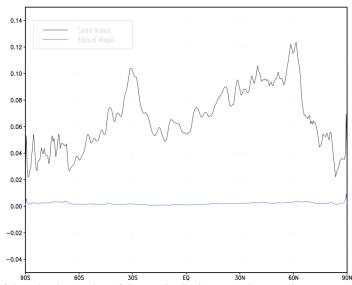


Figure 4.4: Zonal mean of the absolute value of the vertically integrated mass divergence analysis increment.

The manner in which the increment of vertically integrated mass divergence is made to vanish is quite

different, however, between the various cases.

Plots of the zonal mean horizontal wind divergence (Figure 4.5) show that in general that the background state (and subsequent analyses) have significant divergence near the model top, and a secondary maximum near 200 mb. Case 1, however, shows a pathological divergence field near model top due to the inability of Case 1 to scale its adjustments. Case 2 and Case 3 produce divergence fields quite similar to the standard analysis and background states.

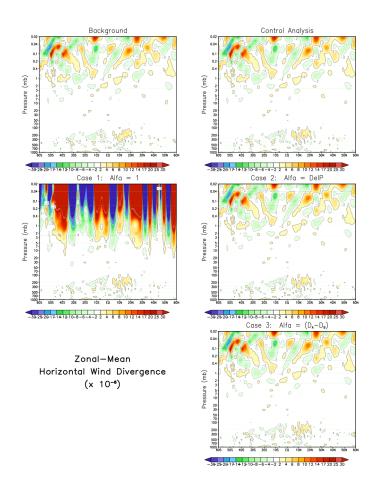


Figure 4.5: The zonal mean horizontal wind divergence (plotted on constant pressure surfaces) of the background state (from the model first guess) and the corresponding results from the analysis states.

Plots of the zonal mean of the analysis increment of divergence (Figure 4.6) again highlight the inherent problems associated with Case 1, while Case 2 and Case 3 look quite reasonable. Notice that Case 3 shows a substantial impact on the overall divergence pattern around 200 hPa.

Figure 4.7 shows the zonal mean of the adjustment made to the control analysis of horizontal divergence. Case 1 makes extremely large adjustments in the upper levels of the model which, when mass-weighted, tend to produce the desired vertically integrated result. Cases 2 and 3 tend to produce changes which are more localized in the troposphere. Case 2 applies small mass-weighted changes uniformly in the vertical,

while Case 3 applies somewhat larger adjustments in regions associated with large analysis increments.

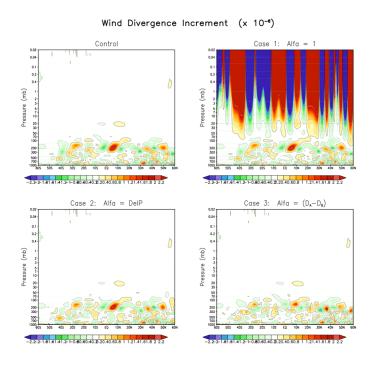


Figure 4.6: The zonal mean of the analysis increment of divergence.

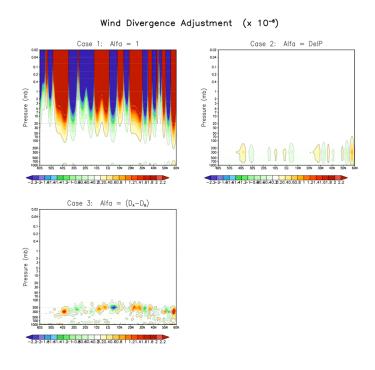


Figure 4.7: The zonal mean of the adjustment made to the control analysis of horizontal divergence.

Finally, the forecasts after 15 minutes of integration using the balanced analysis states corresponding to Case 2 and Case 3 are shown in Figure 4.8, together with the original forecasts from the background and the control analysis. It should again be noted that the initial condition of the mass field for all the analysis states were identical. Only the *divergent* components of the winds were modified for the analysis cases 1 and 2. We see that the forecasts initialized from the balanced analysis states were better able to preserve the low pressure associated with Tropical Storm Chris than the original control analysis.

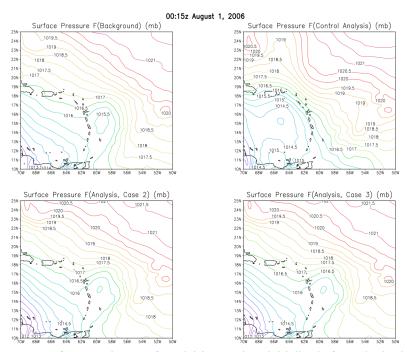


Figure 4.8: Surface pressure after 15 minutes of model integration, initialized from the background and analysis states (Control, Case 2, and Case 3).

5. GEOS-5 Development and Product History

GEOS-5.0.1: The interim operational version of the GEOS-5 DAS, used to generate products for the Aura instrument teams.

GEOS-5.1.0: Addressed deficiencies noted in GEOS-5.0.1 as well as tuning and development issues for the Modern Era Reanalysis for Research Applications (MERRA, e.g., Bosilovich et al., 2006). This system has undergone a formal validation procedure. The validation results will be documented in a separate technical report. This system was used to support the EOS Aura science team reprocessing effort.

GEOS-5.2.0: Addressed deficiencies noted in GEOS-5.1.0 in high latitudes. This is the system used for MERRA, to support the ARCTAS field campaign and the CERES science team. The changes from GEOS-5.1.0 are documented with GEOS-5.1.0.

From 5.0.1 to 5.1.0, substantial changes have been made to both the atmospheric general circulation model (dynamics and physics modules) and analysis system. These modifications operate in concert to impact virtually all output product fields. It is therefore impossible to identify or attempt to quantify one-to-one correspondences between individual system changes and the resulting impacts on the fields. It is clear, however, that the product quality has increased overall, with notable substantial improvements in several key aspects. These include a significantly reduced easterly bias in the upper tropospheric zonal wind along the equator, improved distribution and mean values of precipitation in both the tropics and mid-latitude storm tracks, reduced biases in various land surface quantities, and the elimination of spurious oscillations in both the mid-tropospheric temperature fields at middle to high latitudes and the near-top model level temperature fields near the north pole. The 5.2.0 system addresses a deficiency in the diurnal cycle in the high latitudes.

Updates in 5.1.0

Updates to the GCM

Updates to the Dynamics Module

- 1) Correction for reproducibility of results in the case of the model being run on different processor layouts.
- 2) The Polar Filter has been switched to use an FFT poleward from about the 45th parallel (rather than an FFT near the poles and an algebraic version farther away from poles). The new Polar Filter was implemented to fix a problem encountered if the stratospheric jet crossed the pole during N. Hemisphere Winter.
- 3) A new computation of U10M and V10M were implemented to represent 10-meter winds better, assuming neutral stability.
- 4) A new calculation of diagnostic OMEGA was implemented to be more consistent with the calculated rate of change of kinetic and potential energies.

Updates to the Physics Modules

- 1) Corrected ALBEDO boundary conditions, using new albedo data sets.
- 2) Changed Land-Ice Albedo to 0.75.
- 3) Reduced re-evaporation over land, so that it is the same as over sea.
- 4) Placed a lower limit of 0.4 on the Reynolds number
- 5) Decreased the roughness for heat over bare soil (for values of Leaf Area Index <0.3)
- 6) Fixed out-of-bounds array in IR radiation routine.
- 7) Added protection for LOG(DZ...) in Catchment for thinner levels.

- 8) Limits on the Reynolds Number over ocean grid points were implemented. The upper limit was changed from 1000 to 50; the lower limit changed from 0.4 to 0.1.
- 9) The topography datasets have been modified by multiplicative factors to adjust the global mean value to 231.5m (which is the mean of GTOPO30).
- 10) The MOIST CRF parameter MAX_RI was changed from 110×10^{-6} to 75×10^{-6} to increase the short/long-wave cloud radiative forcing in the mid-levels in the mid-latitude ice clouds.
- 11) The RAS relaxation timescale was changed from one time step (20 minutes) to 12 hrs.
- 12) An upper limit of 2 was imposed on the Richardson Number.
- 13) Modifications were made to include different heat diffusivities over land and over high topography.
- 14) The autoconversion rate was increased above 700 hPa.
- 15) The bounds for the relative humidity ramp for mass flux in RAS were increased from [0.3,0.4] to [0.6,0.8].
- 16) The temperature perturbation in convective boundary layers was capped at 2°K.

Updates to the Land Surface Module

- 1) Updates were implemented to the catchment soil thermal conductivity calculation.
- 2) The surface layer's heat capacity was reduced outside of tropical forests.
- 3) A snow energy accounting variable (HSNACC) was added to output diagnostics. HSNACC accounts, among other things, for the fact that the snowpack (but not the atmosphere) must treat differences in the energy content of snow falling at different temperatures. (HSNACC is an improved version of the older variable HCORR, which had, in the older model only, been added to SHFLUX.)
- 4) The WCHANGE and ECHANGE variables were added to output diagnostics. These variables are, respectively, the change over the timestep of the total water (in kg/m²s) and total energy (in W/m²) in the land surface element.
- 5) Minor issues related to energy and water budget accounting were corrected.
- 6) Minor issues were corrected in the snow code (initialization of snowpack during first snowfall, and re-layering)
- 7) The snow thickness over glaciers has been fixed at 4 m.
- 8) The capacity of canopy interception reservoir was increased by a factor of 5.

Updates to the GCM-Analysis Interface

- 1) Switched from FFT to simple average for D-grid to A-grid transform.
- 2) Fixed a bug in v-wnd in D-grid to A-grid and A-grid to D-grid transforms
- 3) Snow-water-equivalent background file provided for CRTM emissivity calculation in GSI (instead of snow depth)
- 4) Changes in the grid point land/water/ice definition needed for the Radiative Transfer Model and for QC. The grid point is defined as a water grid point if the water fraction of the grid box is > 0.6. The grid point is defined as sea-ice if it is a water grid point and either the ice fraction is > 0.5 or the surface temperature is < -1.7C.
- 5) Updated output routines to handle double precision value for longitude.

Updates to the Analysis

1) Updated to new background error statistics. These new statistics provide an improved mass-wind balance in the tropics and reduce the background error variance for balanced temperature at the lowest model levels over the globe.

- 2) Implemented QC bug fix for MODIS, tightening the tolerance on the gross check quality control to appropriate values.
- 3) MODIS deep-layer clear-sky winds added to input observation stream (after 2006).
- 4) The CQCVAD routine was added to provide quality control checks for Doppler VAD winds.
- 5) Over snow, ice and mixed surfaces the following microwave radiances have been excluded: AMSU-A channels 1-6 and 15; MSU channels 1 and 2; AMSU-B channels 1, 2 and 5.
- 6) A bug fix was implemented for EOS-AMSU-A emissivity calculation. The EOS AMSU-A bug was a logic error which resulted in EOS AMSU-A using a default emissivity calculation instead of the EOS AMSU-A-specific calculation.
- 7) The changing temperature lapse rate option is invoked for the satellite bias correction estimation.
- 8) Implemented a vortex re-locator for tropical cyclones (only). The utility re-positions identified tropical cyclone vortices in the background (model guess) field, in accordance with their observed locations as determined by the National Hurricane Center. Only the position of the vortex position, and not its intensity, is explicitly altered by this utility. The re-positioning improves the use of appropriate observations in the vicinity of the storm and provides a better initial state for the forecast.
- 9) The satellite bias angle correction file was updated for data from 2001 forward.
- 10) The channel selection was updated for AQUA/AIRS and AMSU-B on NOAA-15.
- 11) The impact of all the radiance data on ozone was excluded.

Updates in 5.2.0

Updates to the GCM

Updates to the Physics Module

- 1) A bug in cloudnew. F90 related to the use of the wind shear pdf was corrected.
- 2) Updates were made in cloudnew.F90 to allow a) thicker cold low-level cloud and b) lower limits on RH in re-evaporation.
- 3) Lowered the upper limit on RADQL and RADQI to 1 g/kg from 40 g/kg.
- 4) A bug in MOIST was fixed to pressure weight DTDTFRIC.
- 5) TROPP_THERMAL, TROPP_EPV, and TROPP_BLENDED options were implemented for Tropopause Pressure.
- 6) Moved updating of FR in GEOS_CatchGridComp.F90 to AFTER DTS and DQS computations. This provided consistency with the LSM calculations and prevented excessively large DTS and DQS values.
- 7) Budgets computed in catchment.f90 were fixed.
- 8) Protections against negative values of Q2M, Q10M, SPHU, OX, EKM and EKH were implemented.
- 9) The bounds for the relative humidity ramp for mass flux in RAS were changed from [0.6,0.8] to [0.5,0.65].
- 10) The temperature perturbation in convective boundary layers was capped at 2°K over the ocean and 4°K over the land.
- 11) Corrections were made to ALBEDO and SLRSFC calculations in GEOS_SolarGridComp.F90 and sorad.F.
- 12) The historical CO₂ record is used.
- 13) A gravity wave drag heating correction based on energy conversion from waves (rather than mean flow) was implemented.

Updates to the Land Surface Module

1) The LANDICEALBEDO was changed to 0.775 (from 0.8).

2) Modifications were made to thermal capacity of ice to allow diurnal cycle of surface temperature over land and sea ice.

Updates to the Analysis

- 1) The satellite bias correction was turned off for AMSU-A channel 14 and SSU channel 3.
- 2) CRTM coefficients for AMSU and MSU, all channels for NOAA-8 and SSU channels for NOAA-11 were updated.
- 3) A bug was fixed in the quality control of microwave instruments.

6. References

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Appendix A. AIRS 281 Channel Subset List

Assimilation	Instrument	SRF Centroid
Channel No.	Channel	Frequency
Chamici No.	No.	(cm ⁻¹)
1	1	649.613
2	6	650.807
3	7	651.046
4	10	651.765
5	11	652.005
6	15	652.968
7	16	653.209
8	17	653.450
9	20	654.175
10	21	654.417
11	22	654.659
12	24	655.144
13	27	655.873
14	28	656.116
15	30	656.604
16	36	658.070
17	39	658.806
18	40	659.052
19	42	659.544
20	51	661.767
21	52	662.015
22	54	662.512
23	55	662.761
24	56	663.009
25	59	663.757
26	62	664.507
27	63	664.757
28	68	666.011
29	69	666.262
30	71	666.766
31	72	667.018
32	73	667.270
33	74	667.522
34	75	667.775
35	76	668.028
36	77	668.281
37	78	668.534
38	79	668.787
39	80	669.041
40	82	669.549
41	83	669.803

42 43 44	84	670.058
	96	
11	80	670.567
	92	672.100
45	93	672.357
46	98	673.641
47	99	673.899
48	101	674.414
49	104	675.189
50	105	675.448
51	108	676.226
52	110	676.745
53	111	677.005
54	113	677.526
55	116	678.308
56	117	678.570
57	123	680.142
58	124	680.404
59	128	681.457
60	129	681.721
61	138	689.491
62	139	689.762
63	144	691.119
64	145	691.391
65	150	692.755
66	151	693.029
67	156	694.400
68	157	694.674
69	159	695.225
70	162	696.052
71	165	696.881
72	168	697.712
73	169	697.990
74	170	698.267
75	172	698.824
76	173	699.102
77	174	699.381
78	175	699.660
79	177	700.218
80	179	700.777
81	180	701.057
82	182	701.618

84 186 702.742 85 190 703.870 86 192 704.436 87 198 706.137 88 201 706.991 89 204 707.847 90 207 708.706 91 210 709.566 92 215 711.005 93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 </th <th>83</th> <th>185</th> <th>702.461</th>	83	185	702.461
86 192 704.436 87 198 706.137 88 201 706.991 89 204 707.847 90 207 708.706 91 210 709.566 92 215 711.005 93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236	84	186	702.742
87 198 706.137 88 201 706.991 89 204 707.847 90 207 708.706 91 210 709.566 92 215 711.005 93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789	85	190	703.870
88 201 706.991 89 204 707.847 90 207 708.706 91 210 709.566 92 215 711.005 93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227	86	192	704.436
89 204 707.847 90 207 708.706 91 210 709.566 92 215 711.005 93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485	87	198	706.137
90 207 708.706 91 210 709.566 92 215 711.005 93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014	88	201	706.991
91 210 709.566 92 215 711.005 93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603	89	204	707.847
92 215 711.005 93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 <td>90</td> <td>207</td> <td>708.706</td>	90	207	708.706
93 216 711.293 94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 <td>91</td> <td>210</td> <td>709.566</td>	91	210	709.566
94 221 712.739 95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 </td <td>92</td> <td>215</td> <td>711.005</td>	92	215	711.005
95 226 714.191 96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171<	93	216	711.293
96 227 714.482 97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099	94	221	712.739
97 232 715.941 98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.38	95	226	714.191
98 252 721.838 99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.1	96	227	714.482
99 253 722.135 100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.	97	232	715.941
100 256 723.029 101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843	98	252	721.838
101 257 723.328 102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871	99	253	722.135
102 261 724.524 103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917	100	256	723.029
103 262 724.824 104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918	101	257	723.328
104 267 726.326 105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937	102	261	724.524
105 272 727.834 106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	103	262	724.824
106 295 734.150 107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	104	267	726.326
107 299 735.382 108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	105	272	727.834
108 300 735.690 109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	106	295	734.150
109 305 737.236 110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	107	299	735.382
110 310 738.789 111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	108	300	735.690
111 321 742.227 112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	109	305	737.236
112 325 743.485 113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	110	310	738.789
113 333 746.014 114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	111	321	742.227
114 338 747.603 115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	112	325	743.485
115 355 753.057 116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	113	333	746.014
116 362 755.325 117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	114	338	747.603
117 375 759.574 118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	115	355	753.057
118 453 793.171 119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	116	362	755.325
119 475 801.099 120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	117	375	759.574
120 484 804.386 121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	118	453	793.171
121 497 809.180 122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	119	475	801.099
122 528 820.834 123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	120	484	804.386
123 587 843.913 124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	121	497	809.180
124 672 871.289 125 787 917.306 126 791 918.747 127 843 937.908	122	528	820.834
125 787 917.306 126 791 918.747 127 843 937.908	123	587	843.913
126 791 918.747 127 843 937.908	124	672	871.289
127 843 937.908	125	787	917.306
	126	791	918.747
128 870 948.184	127	843	937.908
	128	870	948.184
129 914 965.431	129	914	965.431

130	950	979.128
131	1003	1001.384
131	1003	1001.384
133	1019	1008.300
134	1024	1010.481
135	1030	1013.109
136	1038	1016.635
137	1048	1021.077
138	1069	1030.528
139	1079	1035.089
140	1082	1036.465
141	1083	1036.924
142	1088	1039.227
143	1090	1040.151
144	1092	1041.077
145	1095	1042.468
146	1104	1056.104
147	1111	1059.444
148	1115	1061.361
149	1116	1061.841
150	1119	1063.285
151	1120	1063.767
152	1123	1065.216
153	1130	1068.610
154	1138	1072.515
155	1142	1074.478
156	1178	1092.451
157	1199	1103.199
158	1206	1106.826
159	1221	1114.675
160	1237	1123.162
161	1252	1131.229
162	1260	1135.575
163	1263	1216.974
164	1266	1218.496
165	1285	1228.225
166	1301	1236.539
167	1304	1238.110
168	1329	1251.357
169	1371	1285.475
170	1382	1291.709
171	1415	1310.766
172	1424	1316.058
173	1449	1330.976
174	1455	1334.605
175	1466	1339.687
176	1477	1345.312
	1	1 12

177	1500	1357.236
178	1519	1367.253
179	1538	1377.426
180	1545	1381.213
181	1565	1392.153
182	1574	1397.135
183	1583	1402.153
184	1593	1407.773
185	1614	1419.726
186	1627	1427.229
187	1636	1432.471
188	1644	1437.164
189	1652	1441.888
190	1669	1468.827
191	1674	1471.910
192	1681	1476.247
193	1694	1484.369
194	1708	1493.215
195	1717	1498.958
196	1723	1502.810
197	1740	1513.832
198	1748	1519.074
199	1751	1521.049
200	1756	1524.352
201	1763	1542.449
202	1766	1544.482
203	1771	1547.882
204	1777	1551.981
205	1780	1554.038
206	1783	1556.101
207	1794	1563.709
208	1800	1567.890
209	1803	1569.989
210	1806	1572.092
211	1812	1576.317
212	1826	1586.259
213	1843	1598.495
214	1852	1605.046
215	1865	2181.495
216	1866	2182.400
217	1868	2184.214
218	1869	2184.214
219		2183.122
	1872	
220	1873	2188.761
221	1876	2191.498
222	1881	2196.075
223	1882	2196.993

224 1883 2197.911 225 1911 2223.936 226 1917 2229.592 227 1918 2230.537 228 1924 2236.225 229 1928 2240.033 230 1937 2248.648 231 1941 2252.497 232 2099 2378.426 233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 245 2114 2393.049 <td< th=""><th></th><th></th><th></th></td<>			
226 1917 2229.592 227 1918 2230.537 228 1924 2236.225 229 1928 2240.033 230 1937 2248.648 231 1941 2252.497 232 2099 2378.426 233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 <td< td=""><td>224</td><td>1883</td><td>2197.911</td></td<>	224	1883	2197.911
227 1918 2230.537 228 1924 2236.225 229 1928 2240.033 230 1937 2248.648 231 1941 2252.497 232 2099 2378.426 233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 <td< td=""><td>225</td><td>1911</td><td>2223.936</td></td<>	225	1911	2223.936
228 1924 2236.225 229 1928 2240.033 230 1937 2248.648 231 1941 2252.497 232 2099 2378.426 233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 <td< td=""><td>226</td><td>1917</td><td>2229.592</td></td<>	226	1917	2229.592
229 1928 2240.033 230 1937 2248.648 231 1941 2252.497 232 2099 2378.426 233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 <td< td=""><td>227</td><td>1918</td><td>2230.537</td></td<>	227	1918	2230.537
230 1937 2248.648 231 1941 2252.497 232 2099 2378.426 233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 252 2121 2399.936 <td< td=""><td>228</td><td>1924</td><td>2236.225</td></td<>	228	1924	2236.225
231 1941 2252.497 232 2099 2378.426 233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 252 2121 2399.936 253 2122 2400.923 <td< td=""><td>229</td><td>1928</td><td>2240.033</td></td<>	229	1928	2240.033
232 2099 2378.426 233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 252 2121 2399.936 253 2122 2400.923 254 2123 2401.911 <td< td=""><td>230</td><td>1937</td><td>2248.648</td></td<>	230	1937	2248.648
233 2100 2379.395 234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 252 2121 2399.936 253 2122 2400.923 254 2123 2401.911 255 2128 2406.863 <td< td=""><td>231</td><td>1941</td><td>2252.497</td></td<>	231	1941	2252.497
234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 252 2121 2399.936 253 2122 2400.923 254 2123 2401.911 255 2128 2406.863 256 2134 2412.832 <td< td=""><td>232</td><td>2099</td><td>2378.426</td></td<>	232	2099	2378.426
234 2101 2380.365 235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 252 2121 2399.936 253 2122 2400.923 254 2123 2401.911 255 2128 2406.863 256 2134 2412.832 <td< td=""><td>233</td><td>2100</td><td>2379.395</td></td<>	233	2100	2379.395
235 2103 2382.308 236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 252 2121 2399.936 253 2122 2400.923 254 2123 2401.911 255 2128 2406.863 256 2134 2412.832 257 2141 2419.835 <td< td=""><td>234</td><td>2101</td><td>2380.365</td></td<>	234	2101	2380.365
236 2104 2383.280 237 2106 2385.227 238 2107 2386.202 239 2108 2387.178 240 2109 2388.154 241 2110 2389.132 242 2111 2390.110 243 2112 2391.089 244 2113 2392.068 245 2114 2393.049 246 2115 2394.030 247 2116 2395.012 248 2117 2395.995 249 2118 2396.979 250 2119 2397.964 251 2120 2398.949 252 2121 2399.936 253 2122 2400.923 254 2123 2401.911 255 2128 2406.863 256 2134 2412.832 257 2141 2419.835 258 2145 2446.195 <td< td=""><td></td><td></td><td></td></td<>			
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271	2328	2611.066
272	2333	2616.383
273	2339	2622.792
274	2348	2632.466
275	2353	2637.872
276	2355	2640.041
277	2357	2642.214
278	2363	2648.752
279	2370	2656.423
280	2371	2657.522
281	2377	2664.138

Appendix B. Observational Error Variances for Satellite Radiances

The observational (instrument and representativeness) error variance for various radiance channels used in the GSI analysis system.

Table B1: TOVS

Satellite	Instrument/Channel	R = instrument +
		representativeness variance (°C) ²
NOAA-14	HIRS channel 2	0.410
	HIRS channel 3	0.360
	HIRS channel 4	0.250
	HIRS channel 5	0.245
	HIRS channel 6	0.360
	HIRS channel 7	0.470
	HIRS channel 8	1.000
	HIRS channel 9	1.000
	HIRS channel 10	0.500
	HIRS channel 11	1.000
	HIRS channel 12	1.500
	HIRS channel 13	0.464
	HIRS channel 14	0.390
	HIRS channel 15	0.320
	MSU channel 2	0.305
	MSU channel 3	0.240
	MSU channel 4	0.290
NOAA-15	HIRS channel 2	0.410
	HIRS channel 3	0.360
	HIRS channel 4	0.250
	HIRS channel 5	0.245
	HIRS channel 6	0.360
	HIRS channel 7	0.470
	HIRS channel 8	1.000
	HIRS channel 9	1.000
	HIRS channel 10	0.500
	HIRS channel 11	1.000
	HIRS channel 12	1.500
	HIRS channel 13	0.464
	HIRS channel 14	0.390
	HIRS channel 15	0.320
	AMSU-A channel 1	4.500
	AMSU-A channel 2	4.500
	AMSU-A channel 3	4.500
	AMSU-A channel 4	0.600
	AMSU-A channel 5	0.300

AMSU-A channel 6	0.200
AMSU-A channel 7	0.250
AMSU-A channel 8	0.275
AMSU-A channel 9	0.300
AMSU-A channel 10	0.400

Table B2: GOES

Satellite	Instrument/Channel	R = instrument +
		representativeness variance (°C) ²
GOES-8	HIRS channel 1	4.500
	HIRS channel 2	0.410
	HIRS channel 3	0.360
	HIRS channel 4	0.250
	HIRS channel 5	0.245
	HIRS channel 6	0.360
	HIRS channel 7	0.470
	HIRS channel 8	1.000
	HIRS channel 9	1.500
	HIRS channel 10	0.500
	HIRS channel 11	1.000
	HIRS channel 12	1.500

Appendix C. Acronyms

3DVar Three-dimensional Variational assimilation AGCM Atmospheric General Circulation Model

AIREP AIRcraft REPort

AIRS Advanced Infrared Sounder (on Aqua)

AMSU Advanced Microwave Sounding Unit (on later TIROS)
AMV Atmospheric Motion Vectors (also called CTW)

AQUA EOS PM satellite

ASDAR Aircraft to Satellite DAta Relay system

AURA EOS CHEM satellite
ATOVS Advanced TOVS

AVHRR Advanced Very High Resolution Radiometer

BUFR Binary Universal Form for the Representation of meteorological data

CAPE Convective Available Potential Energy

CLSM Catchment Land Surface Model
C-MAN Coastal-Marine Automated Network
CRTM Community Radiative Transfer Model
CTW Cloud Track Wind (now called AMV)

DAS Data Assimilation System
DEM Digital Elevation Model

DMSP Defense Meteorological Satellite Program

DU Dobson Unit (Ozone amount in atmospheric column)
ECMWF European Centre for Medium Range Weather Forecasting

ELW Expanded Low-resolution Winds

EOS Earth Observing System

ERS-1,2 Environmental Research Satellite (surface winds obtained using the AMI, Active

Microwave Unit)

ESMF Earth System Modeling Framework

EUMETSAT European Organisation for the Exploitation of Meteorological Satellites

fvGCM Finite-volume General Circulation Model GCM General Circulation Model (Atmospheric)

GEOS Goddard Earth Observing System

GLATOVS Goddard Laboratory for Atmospheres TOVS (radiative transfer model)

GMAO Global Modeling and Assimilation Office (GSFC)

GMS Geostationary Meteorological Satellite

GOES Geosynchronous Operational Environmental Satellite

GSFC (NASA) Goddard Space Flight Center GSI Grid-point Statistical Interpolation

GTOPO30 Global Digital Elevation Model (DEM), 30 arc second resolution

GTS Global Telecommunication System
HALOE Halogen Occultation Experiment
HIRS2,3,4 High-resolution Infrared Spectrometer

HSB Humidity Sounder for Brazil IAU Incremental Analysis Updating

IR Infra-Red

IRSSE Infra-Red Sea Surface Emissivity

JCSDA Joint Center for Satellite Data Assimilation

JMA Japan Meteorological Agency LCV Lagrangian Control Volume

LSM Land Surface Model

MDCRS Meteorological Data Collection and Reporting System

MERRA Modern Era Retrospective-analysis for Research and Applications

METAR Aviation routine weather report MHS Microwave Humidity Sounder MLS Microwave Limb Sounder

MODIS Moderate Resolution Imaging Spectroradiometer

MPI Message Passing Interface

MSU Microwave Sounding Unit (part of TOVS)

MW MicroWave

NASA National Aeronautics and Space Administration NCEP National Centers for Environmental Prediction

NESDIS National Environmental Satellite, Data, and Information Service

NEXRAD Next generation Radar

NMC National Meteorological Center

NOAA National Oceanic and Atmospheric Administration

NPN NOAA Profiler Network
NWP Numerical Weather Prediction

OMF(O-F) Observation Minus Background (or First Guess)
OSS Optimal Spectral Sampling (radiative transfer method)

PAOBS Synthetic surface Pressure OBS PAR Photosynthetically Active Radiation

PBL Planetary Boundary Layer

PDF Probability Distribution Function

PIBAL PILot BALloon

PILPS Project for the Intercomparison of Land-surface Parameterization Schemes

PIREP PIlot REPort

POES Polar-Orbiting Environment Satellite

QC Quality Control QM Quality Marker

RAS Relaxed Arakawa-Schubert RFF Recursive Filter Flag RH Relative Humidity

Rhone-AGG Rhone AGGregation Experiment

RTM Radiative Transfer Model

SARTA Stand-alone AIRS Radiative Transfer Algorithm SBUV/2 Solar Backscatter Ultraviolet Spectral Radiometer-2

SQC Statistical Quality Control

SSM/I Special Sensor Microwave/Imager (on DMSP satellites)

SSI Spectral Statistical Interpolation

SSU Stratospheric Sounding Unit (superseded by AMSU)

TERRA EOS AM Satellite

TIROS Television and Infrared Observatory Spacecraft

TLM Tangent Linear Model
TMI TRMM Microwave Imager

TOMS Total Ozone Mapping Spectrometer TOVS TIROS Operational Vertical Sounder

TPW Total Precipitable Water

TRMM Tropical Rainfall Measurement Mission

UTC Coordinated Universal Time

UV Ultra-violet

VAD

VIS

Velocity Azimuth Display wind Visible World Meteorological Organization Weather Surveillance Radar 88 Doppler WMO WSR-88D

WV Water Vapor

Appendix D. Acknowledgements

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